



# Magnetosheath plasma flow model around Mercury

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## Abstract.

The magnetosheath is defined as the plasma region between the bow shock, where the super-magnetosonic solar wind plasma is decelerated and heated, and the outer boundary of the intrinsic planetary magnetic field, the so called magnetopause. Based on the Soucek-Escoubet magnetosheath flow model at Earth, we present the first analytical magnetosheath plasma flow model for Mercury. It can be used to estimate the plasma flow magnitude and direction at any given point in the magnetosheath exclusively on the basis of the plasma parameters of the upstream solar wind. The aim of this paper is to provide a tool to back-trace the magnetosheath plasma flow between multiple observation points or from a given spacecraft location to the bow shock.

## 1 Introduction

The magnetosphere of a planet constitutes an obstacle to the super-magnetosonic solar wind. Upstream of the planet a bow shock emerges, because the interplanetary magnetic field (IMF), embedded in the solar wind, cannot simply penetrate the magnetosphere. At the bow shock the super-magnetosonic solar wind plasma is decelerated and heated. The region with the subsonic, heated plasma downstream of the bow shock is called magnetosheath. The magnetosheath plays an important role in the interaction between bow shock and magnetosphere as it conveys energy between the solar wind and the planetary magnetosphere.

One of the earliest magnetosheath plasma flow models is the hydrodynamic model introduced by Spreiter *et al.* (1966). Basically the model solves the gas-dynamic differential equations of an unmagnetized fluid around an obstacle, represented by the magnetosphere. It has successfully been tested against in-situ spacecraft data (Song *et al.*, 1999; Stahara *et al.*, 1993; Spreiter and Alksne, 1968) and applied to model the magnetospheres of various planets in our solar system (see Stahara, 2002, for a review). A decisive drawback of this model, however, is the high complexity and computational demands to calculate numerically a set of differential equations.

To reduce the computational complexity, several analytical plasma flow models have alternatively been proposed (Russell *et al.*, 1983; Kallio and Koskinen, 2000; Romashets *et al.*, 2008). An analytical magnetosheath flow model, which has successfully been tested against spacecraft observations at Earth, has been implemented by Soucek and Escoubet (2012). This model



25 is based on the magnetic field model developed by *Kobel and Flückiger* (1994) and later modified and extended by *Génot et al.* (2011) to obtain a magnetosheath plasma flow model. The essential advantage of this model is its compatibility with a wide range of bow shock and magnetopause models while retaining the simplicity and computational efficiency of the original magnetic field model. Furthermore, the model allows to calculate the plasma flow velocity at any point in the magnetosheath using only the spacecraft position and solar wind parameter upstream of the bow shock.

30 In this work we follow the procedure proposed by *Soucek and Escoubet* (2012) and rescale their terrestrial magnetosheath flow model to the space environment at Mercury. First, we introduce the Hermean bow shock and magnetopause model, used to obtain the magnetosheath plasma flow model. Second, we revisit the magnetic field model of *Kobel and Flückiger* (1994) which *Soucek and Escoubet* (2012) used to determine the plasma velocity direction in the magnetosheath. Third, we extend the model by the Rankine-Hugoniot relations in a similar way as *Génot et al.* (2011) to determine the velocity magnitude  
35 downstream of the shock.

The aim of this paper is to provide a tool to estimate the plasma flow at a given point of spacecraft observation inside the Hermean magnetosheath on the basis of the solar wind conditions.

## 2 Bow shock and magnetopause model at Mercury

In the following we use an aberrated Mercury Solar Magnetospheric (MSM) coordinate system. This coordinate system is  
40 based on the Mercury Solar Orbital (MSO) coordinate system, but its origin is shifted northward by 479 km from the MSO origin to account for Mercury's dipole offset and rotated into the solar wind velocity direction. In the MSO coordinate system the  $X_{\text{MSO}}$ -axis points sunward, the  $Y_{\text{MSO}}$ -axis points anti-parallel to Mercury's orbital velocity, and  $Z_{\text{MSO}} = X_{\text{MSO}} \times Y_{\text{MSO}}$  completes the right-handed system. To compensate for the aberration of the solar wind direction due to the orbital motion of Mercury around the sun, the  $X_{\text{MSO}}$ -axis is rotated anti-parallel to the solar wind flow velocity direction. In the MSM coordinate  
45 system the bow shock and magnetopause models are considered to be cylindrically symmetric around the  $X_{\text{MSM}}$ -axis, reducing the three dimensions  $\{X_{\text{MSM}}, Y_{\text{MSM}}, Z_{\text{MSM}}\}$  to two dimensions  $\{X_{\text{MSM}}, \rho_{\text{MSM}}\}$  with  $\rho = \sqrt{Y_{\text{MSM}}^2 + Z_{\text{MSM}}^2}$ .

*Slavin et al.* (2009) modeled the bow shock at Mercury by a conic section of the form

$$\xi = \sqrt{(x_{BS} - x_0)^2 + \rho_{BS}^2} = \frac{p\epsilon}{1 + \epsilon \cos \phi}, \quad (1)$$

with  $x_0$  the distance of the focus of the conic section from the dipole center along  $X_{\text{MSM}}$ ,  $\rho_{BS} = \sqrt{y_{BS}^2 + z_{BS}^2}$  the distance  
50 from the  $X_{\text{MSM}}$ -axis,  $p$  the focal parameter, and  $\epsilon$  the eccentricity. With the advent of the MESSENGER (MERcury Surface, Space ENVironment, GEophysics and Ranging *Solomon et al.*, 2007) spacecraft in an orbit around Mercury, it was possible to characterize the spatial location of the bow shock and magnetopause statistically. *Winslow et al.* (2013) determined that the best-fit parameters to the bow shock are given by  $x_0 = 0.5 R_{\text{M}}$ ,  $p = 2.75 R_{\text{M}}$  and  $\epsilon = 1.04$ . With these parameters the extrapolated subsolar bow shock stand-off distance is  $R_{\text{BS}} = 1.9 R_{\text{M}}$  (Mercury radii,  $1 R_{\text{M}} \sim 2440$  km). For this work it is



55 advantageous to transform Equation (1) into the origin of the MSM coordinate system with

$$\begin{aligned} r_{BS} &= \sqrt{(\xi \cos \phi + x_0)^2 + (\xi \sin \phi)^2}, \\ \theta &= \cos^{-1} \left( \frac{\xi \cos \phi}{r_{BS}} \right), \end{aligned} \quad (2)$$

where  $r_{BS}$  is the distance from the dipole center to the bow shock and  $\theta$  the angle between  $r_{BS}$  and the  $X_{MSM}$ -axis. Figure 1 shows a schematic illustration of the parameters  $\xi$ ,  $\phi$ ,  $r_{BS}$  and  $\theta$ , which are used in the formulation of the bow shock.

60 *Korth et al. (2015)* used the magnetopause model proposed from *Shue et al. (1997)* and found that the MESSENGER observations of magnetopause crossing are best-fit by

$$r_{MP} = \sqrt{x_{MP}^2 + \rho_{MP}^2} = R_{MP} \left( \frac{2}{1 + \cos \theta} \right)^\alpha, \quad (3)$$

with  $\alpha = 0.5$  the best-fit flaring parameter, and  $R_{MP} = 1.42 R_M$  the subsolar stand-off magnetopause distance.

Figure 1 shows the the bow shock (S09-BS) and magnetopause (K15-MP) evaluated from Equations (2) and (3), respectively.

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### 3 The KF94 magnetic field model

To obtain the magnetosheath plasma flow direction we follow the procedure proposed by *Soucek and Escoubet (2012)* and use the magnetic field model developed by *Kobel and Flückiger (1994)*. In the following we denote this model as KF94-model and mark all quantities pertaining to the KF94-model by a tilde  $\tilde{\cdot}$ . In the KF94-model the bow shock (BS) and magnetopause (MP)

70 at Mercury are modeled by parabolic surfaces at a common focus with

$$\tilde{r}_{\{BS,MP\}} = \frac{-\cos \theta + \sqrt{\cos^2 \theta + 4R_{\{BS,MP\}} b_{\{BS,MP\}} \sin^2 \theta}}{2b_{\{BS,MP\}} \sin^2 \theta}, \quad (4)$$

with  $b_{BS} = 1/(4R_{BS} - 2R_{MP})$  and  $b_{MP} = 1/(2R_{MP})$  defined by the stand-off distances  $R_{\{BS,MP\}}$ .

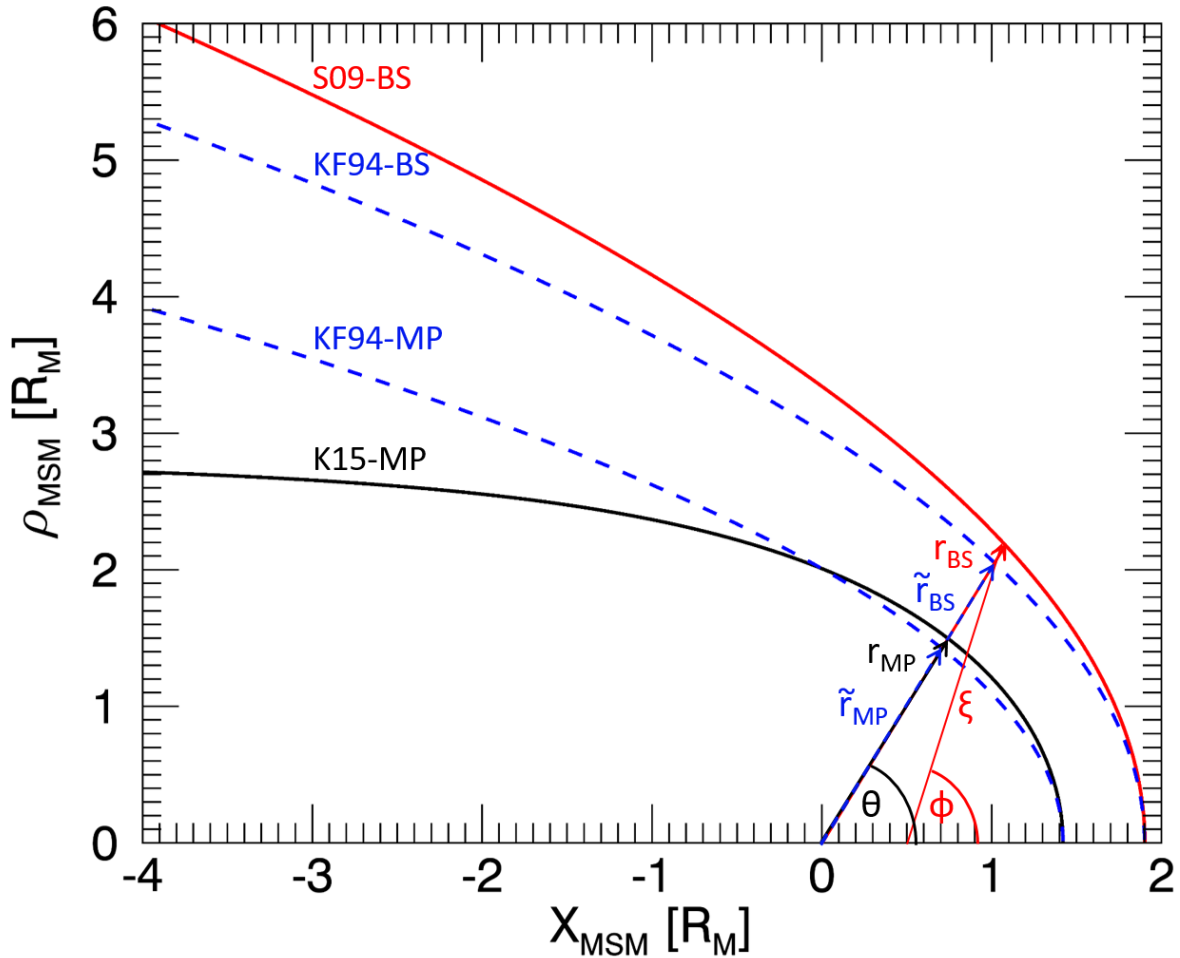
Under the assumption that the IMF is parallel to the solar wind, the magnetic field lines of the KF94-model represent the flowlines of the solar wind and magnetosheath plasma. Using the magnetic field vector direction in the KF94-model, *Soucek*

75 *and Escoubet (2012)* determined the flow velocity vector at a given position  $\mathbf{r} = (x, \rho)$  by

$$\begin{aligned} \tilde{v}_x &= v_m (C/2d - C/R_{MP}), \\ \tilde{v}_\rho &= v_m (C\rho/[2d(d+x - R_{MP}/2)]), \end{aligned} \quad (5)$$

where  $v_m$  corresponds to the flow velocity magnitude,  $d = |\mathbf{r} - \mathbf{r}_0|$  the difference between the given position in the magnetosheath and the parabolic surface focus  $\mathbf{r}_0 = (R_{MP}/2, 0)$ , and  $C = R_{MP}(2R_{BS} - R_{MP})/(2R_{BS} - 2R_{MP})$  a constant defined

80 by the bow shock and magnetopause stand-off distances.



**Figure 1.** Schematic representation of the parameters used in the formulation of the bow shock and magnetopause in the MSM equatorial plane. The solid red line is the bow shock evaluated from Equation (2) (S09-BS, *Slavin et al.*, 2009). The solid black line represents the magnetopause determined by Equation (3) (K15-MP, *Korth et al.*, 2015). The dashed blue lines are the bow shock and magnetopause determined by Equation (4) from the KF94-model (*Kobel and Flückiger*, 1994).

#### 4 The magnetosheath plasma flow model around Mercury

To obtain the magnetosheath plasma flow at a specific point ( $\mathbf{r} = (x, \rho)$ ) in the magnetosheath at Mercury, we evaluate the plasma flow direction first, and then determine the magnitude of the velocity vector from the Rankine-Hugoniot relation across the bow shock.



#### 85 4.1 Plasma flow direction

Following the procedure proposed by *Soucek and Escoubet* (2012), we rescale the plasma flow direction from the KF94-model to Mercury's space environment as follows:

1. As a first step we calculate the angle  $\theta = \cos^{-1}(x/\sqrt{x^2 + \rho^2})$  between  $\mathbf{r}$  and the  $X_{\text{MSM}}$ -axis.

2. Then we estimate the fractional distance,  $\mathcal{F}$ , of  $\mathbf{r}$  between the bow shock and magnetopause from Equations (2) and (3)  
 90 with

$$\mathcal{F} = \frac{r(\theta) - r_{\text{BS}}(\theta)}{r_{\text{BS}}(\theta) - r_{\text{MP}}(\theta)}. \quad (6)$$

3. Now we change into the KF94-model and calculate  $\tilde{r}_{\text{BS}}(\theta)$  and  $\tilde{r}_{\text{MP}}(\theta)$  from Equation (4) with the angle  $\theta$ . Note that the stand-off distances ( $R_{\text{BS}}$  and  $R_{\text{MP}}$ ) and the focus ( $\mathbf{r}_0 = (R_{\text{MP}}/2, 0)$ ) in Equation (4) are the best-fit values from Equations (2) and (3).

95 4. In a next step we determine the fractional position within the magnetosheath in the KF94-model with

$$\tilde{r}(\theta) = \mathcal{F}[\tilde{r}_{\text{BS}}(\theta) - \tilde{r}_{\text{MP}}(\theta)] + \tilde{r}_{\text{BS}}(\theta), \quad (7)$$

according to Equation (6).

5. Using Equation (5) we evaluate the KF94 flow velocity vector,  $\tilde{\mathbf{v}}$ , at the position  $\tilde{r}(\theta)$ . Note that the velocity magnitude  $v_{\text{m}}$  is determined in a later step.

100 6. With the obtained flow velocity vector,  $\tilde{\mathbf{v}}$ , we are able to estimate the new position of an adjacent point along the same flowline  $\mathbf{r}' = \tilde{\mathbf{r}} + \tilde{\mathbf{v}}\Delta t$ , by choosing an infinitesimally small time increment  $\Delta t$ .

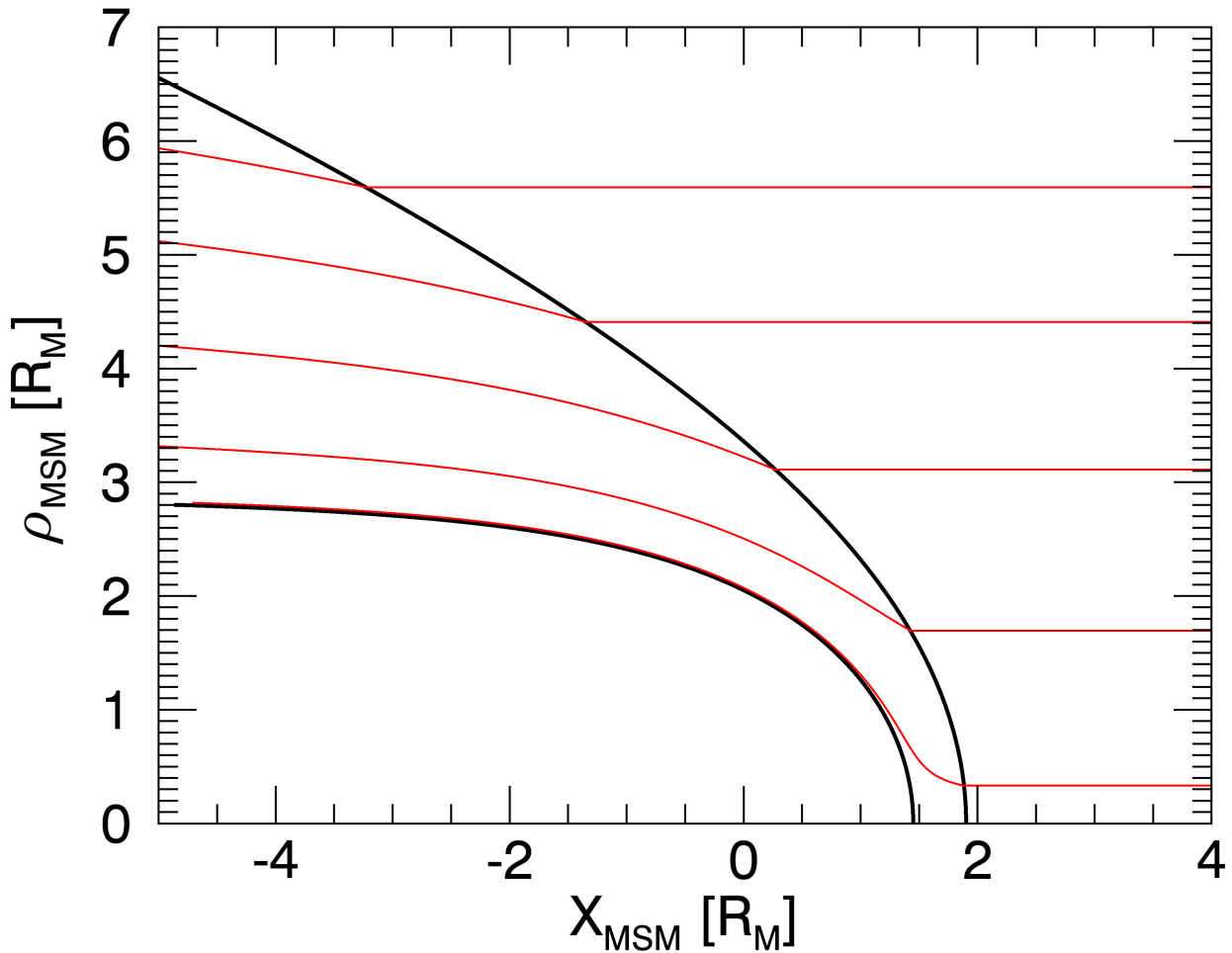
7. Next we determine the angle between the new position and the  $X_{\text{MSM}}$ -axis,  $\theta'$ , and the fractional distance inside the KF94 magnetosheath,  $\mathcal{F}'$ , using Equation (6).

105 8. Finally we transform the new position  $\tilde{\mathbf{r}}'(\theta')$  back from the KF94-model to the original MSM reference frame where the magnetosheath is confined by Equations (2) and (3). The new position,  $\mathbf{r}'$ , inside this magnetosheath is then given by

$$\mathbf{r}' = \mathcal{F}'[\mathbf{r}_{\text{BS}}(\theta') - \mathbf{r}_{\text{MP}}(\theta')] + \mathbf{r}_{\text{BS}}(\theta'), \quad (8)$$

and thus the plasma flow direction can be determined by  $\mathbf{v} = (\mathbf{r}' - \mathbf{r})/\Delta t$ .

Applying recursively this procedure (step(1)-(8)) yields the plasma flowline within Mercury's magnetosheath. In Fig.2 five examples of flowlines are shown.



**Figure 2.** Schematic representation of the flowlines (red) in the MSM equatorial plane. The solid black lines are the bow shock and magnetopause evaluated from Equations (2) and (3), respectively.

#### 110 4.2 Plasma flow magnitude

To evaluate the magnetosheath plasma velocity magnitude,  $v_m$ , we apply the Rankine-Hugoniot (RH) equations, which relate the upstream ( $u$ ) with the downstream ( $d$ ) plasma conditions. The downstream plasma flow velocity directly behind the bow shock,  $v^d$ , is derived by the following procedure:

1. From the given spacecraft position in the magnetosheath,  $\mathbf{r} = (x, \rho)$ , we trace the flowline back to the bow shock. There to  
 115 we iteratively apply steps (1)-(8) from above, with reversed increments  $\tilde{\mathbf{r}}' = \tilde{\mathbf{r}} - \tilde{\mathbf{v}}\Delta t$  in step (6), until the bow shock is



reached ( $\mathcal{F}' = 0$ ). Then we calculate the angle  $\theta_{\text{BS}}$  between the  $X_{\text{MSM}}$ -axis and the bow shock intersection at  $(x_{\text{BS}}, \rho_{\text{BS}})$  with  $\theta_{\text{BS}} = \cos^{-1}(x_{\text{BS}}/\sqrt{x_{\text{BS}}^2 + \rho_{\text{BS}}^2})$ .

2. In a next step we determine the bow shock tangent  $\hat{\mathbf{t}}$  and normal  $\hat{\mathbf{n}}$  unit vectors where the back-traced flowline intersects the bow shock. For any point along the bow shock, the normal,  $\mathbf{n}$ , and tangent,  $\mathbf{t}$ , vector can easily be computed by

$$\begin{aligned} \mathbf{t} &= \left[ \frac{dr_{\text{BS}}}{d\theta} \cos\theta - r_{\text{BS}} \sin\theta \right] \hat{\mathbf{e}}_x + \left[ \frac{dr_{\text{BS}}}{d\theta} \sin\theta + r_{\text{BS}} \cos\theta \right] \hat{\mathbf{e}}_\rho, \\ \mathbf{n} &= \left[ \frac{dr_{\text{BS}}}{d\theta} \sin\theta + r_{\text{BS}} \cos\theta \right] \hat{\mathbf{e}}_x - \left[ \frac{dr_{\text{BS}}}{d\theta} \cos\theta + r_{\text{BS}} \sin\theta \right] \hat{\mathbf{e}}_\rho, \end{aligned} \quad (9)$$

where  $\frac{dr_{\text{BS}}}{d\theta}$  is numerically calculated from two consecutive points along the bow shock given by Equation (2). The shock reference of frame is then defined by the normalized normal and tangent vector at  $\theta_{\text{BS}}$ .

3. In the shock reference frame the RH-equations can be combined to determine the downstream velocity vector component parallel  $v_n^d$  and perpendicular  $v_t^d$  to the shock normal (see e.g. Génot, 2008)

$$\begin{aligned} v_n^d &= v_n^u \frac{1}{\mathcal{R}}, \\ v_t^d &= v_n^u \left( \tan\theta_{\text{Vn}} + \frac{1 - 1/\mathcal{R}}{[M_A^{u2}/(\mathcal{R}\cos^2\theta_{\text{Bn}})] - 1} \tan\theta_{\text{Bn}} \right), \end{aligned} \quad (10)$$

where  $v_n^u$  is the upstream velocity vector component parallel to the shock normal,  $\mathcal{R} = \rho^d/\rho^u$  the compression ratio between the upstream and downstream mass density,  $\theta_{\text{Vn}} = \tan^{-1}(v_t^u/v_n^u)$  the angle between the upstream velocity vector and the shock normal,  $\theta_{\text{Bn}} = \tan^{-1}(B_t^u/B_n^u)$  the angle between upstream magnetic field vector and shock normal, and  $M_A^u = v_n^u \frac{\sqrt{\mu_0 \rho^u}}{B_n^u}$  the upstream Alfvén Mach number with respect to the shock normal.

4. In Equation (10) all parameters pertain to the upstream side, except the compression ratio  $\mathcal{R}$ . However,  $\mathcal{R}$  can also be expressed by exclusively upstream parameters with (see e.g. Anderson, 1963)

$$\begin{aligned} (M_A^{u2} - \mathcal{R})^2 (\gamma \beta^u \mathcal{R} + M_A^{u2} \cos^2 \theta_{\text{Bn}} [(\gamma - 1)\mathcal{R} - (\gamma + 1)]) + \\ \mathcal{R} M_A^{u2} \sin^2 \theta_{\text{Bn}} ([\gamma + (2 - \gamma)\mathcal{R}] M_A^{u2} + \mathcal{R} [(\gamma - 1)\mathcal{R} - (\gamma + 1)]) = 0 \end{aligned} \quad (11)$$

where  $\beta^u = (2\mu_0 p^u)/B^{u2}$  is the ratio of the upstream thermal to magnetic pressures, and  $\gamma$  the polytropic index which is typically assumed to be  $\gamma = 5/3$ .

5. By solving Equation (4) for  $\mathcal{R}$  the downstream velocity magnitude  $v_d = \sqrt{v_n^{d2} + v_t^{d2}}$  is therefore entirely determined by only the upstream plasma parameters.

140 Since the detailed density profile along the flowline is unknown, we assume in a first approximation a constant plasma density and thus a constant velocity magnitude along the flowline. Therefore, the velocity magnitude at a given point  $\mathbf{r}$ , directly



corresponds to the velocity magnitude downstream of the shock and  $v_m = v_d$ . Although this assumption has the tendency to underestimate the velocity close to the magnetopause, it yields satisfactory results in a first approach (Génot *et al.*, 2011).

The entire procedure from above is implemented in an IDL computer program which can be retrieved from OSF (Schmid, 2020). The program is designed to evaluate the plasma flow velocity vector at a given observation point of a spacecraft inside the Hermean magnetosheath exclusively on basis of the upstream solar wind conditions. As the solar wind input parameters we use the solar wind propagation model of Tao *et al.* (2005) which is modified by the orbital motion of Mercury (Acton, 1996). In Fig.3 the results of the model are shown for the average solar wind plasma parameters during the entire MESSENGER operation service between 2011 and 2015. After modifying the solar wind velocity vector of the Tao *et al.* (2005) model by the orbital motion of Mercury (Acton, 1996), the average input solar wind plasma parameters for our model are:  $n^u \approx 40 \text{ cm}^{-3}$ ,  $T \approx 18 \text{ eV}$ ,  $|\mathbf{v}^u| \approx -400 \text{ km/s}$ ,  $|\mathbf{B}^u| \approx 20 \text{ nT}$ ,  $\theta_{Vn} \approx 25^\circ$ , and  $\theta_{Bn} \approx 7^\circ$ . Color coded is the obtained velocity magnitude  $v_m$ . Additionally, the back-traced flowline from a virtual spacecraft located at  $x_{\text{MSM}} = -3 R_M$  and  $\rho_{\text{MSM}} = 3 R_M$  is plotted (green line). At the bow shock intersection the calculated shock normal  $\hat{\mathbf{n}}$  and tangent  $\hat{\mathbf{t}}$  are illustrated in thin black lines. The thick black line downstream of the bow shock shows the velocity vector direction evaluated from the RH relations, which is in good agreement with the streamline direction determined by the KF94-model. At the virtual spacecraft position the model predicts a magnetosheath plasma flow velocity of  $v_x \approx -200 \text{ km/s}$  and  $v_\rho \approx 17 \text{ km/s}$ .

## 5 Discussion and Conclusions

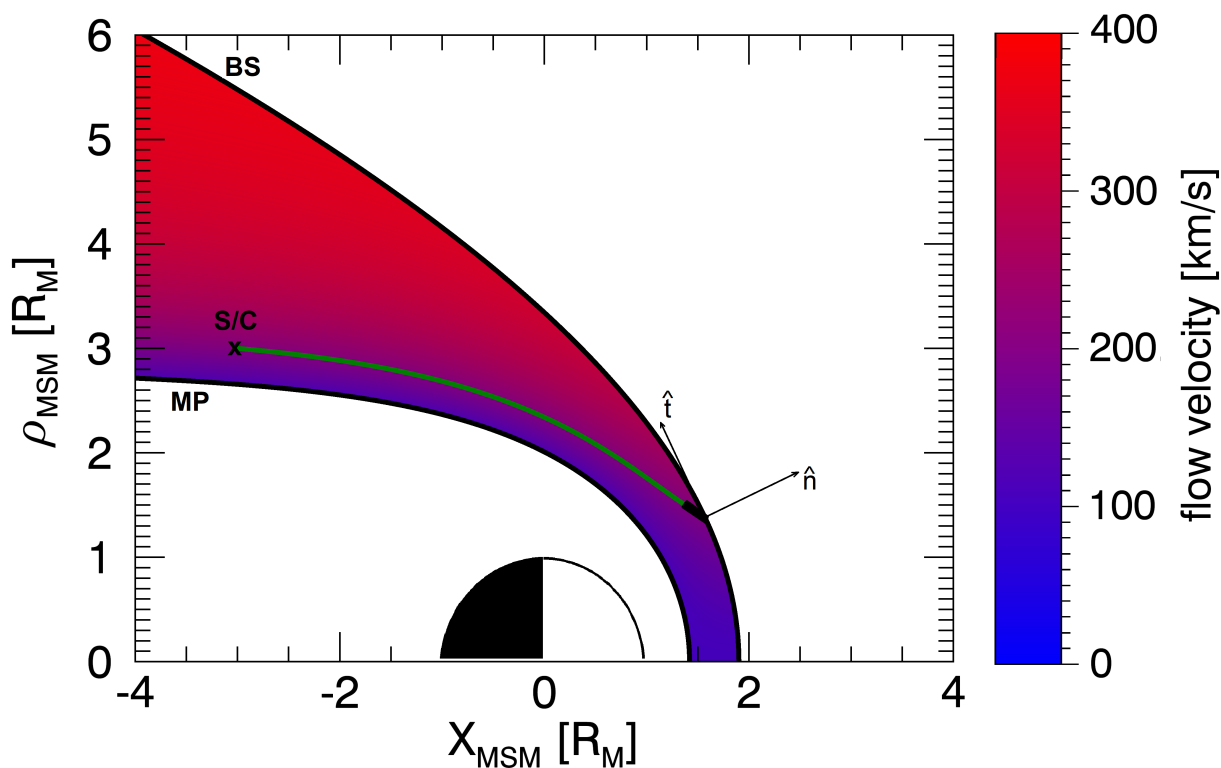
Here we present the first analytical magnetosheath plasma flow model for the space environment around Mercury. The model is based Soucek and Escoubet (2012) magnetosheath model, which has successfully been tested against spacecraft observations at Earth. The proposed model is relatively simple to implement and provides the possibility to trace the flowlines inside the Hermean magnetosheath.

Although the proposed model has a good performance overall for a wide range of upstream conditions, the accuracy strongly depends on the used bow shock and magnetopause model. Here we utilize the bow shock and magnetopause model from Slavin *et al.* (2009) and Korth *et al.* (2015), which were adopted from MESSENGER boundary crossing observations.

The presented model is cylindrically symmetric around the  $X_{\text{MSM}}$ -axis. In reality, however, non-radial IMF conditions will lead to a spatially asymmetric magnetosheath (Nishino *et al.*, 2008; Dimmock and Nykyri, 2013; Dimmock *et al.*, 2016). On the quasi-perpendicular side, where the shock-normal angles  $\theta_{Bn}$  are greater than  $45^\circ$ , the magnetosheath is known to be thicker with larger plasma flow velocities than on the quasi-parallel side, where  $\theta_{Bn} < 45^\circ$ . Such asymmetries cannot be reproduced by the simple model presented here, but should be addressed in future work.

Furthermore, the method used to determine the flow velocity magnitude can possibly be improved. Here we assumed a constant plasma density along the flowline which has the tendency to underestimate the plasma velocity in regions with lower densities e.g. close to the magnetopause. Génot *et al.* (2011) proposed a simple ad-hoc model of a plasma density profile which has been implemented by Soucek and Escoubet (2012). While this ad-hoc density model showed good correspondence with in-situ spacecraft plasma observation at Earth, the solar wind and magnetospheric conditions at other planets can be very different





**Figure 3.** Color-coded flow speed calculated from Equation (10) with the averaged upstream parameters from the *Tao et al. (2005)* solar wind propagation model at Mercury between 2011 and 2015. Also plotted is a schematic representation of back-traced flowline (green) from a virtual spacecraft (S/C) to the bow shock (BS) with the respective shock normal  $\hat{n}$  and tangent  $\hat{t}$  obtained from Equation (9). The thick black line downstream of the BS is the downstream velocity vector direction determined by Equation (10).

175 (like e.g. at Mercury) and thus might give a worse prediction (*Soucek and Escoubet, 2012*). At this stage we decided not to  
 include an ad-hoc density profile, also because it can hardly be tested due to the limited plasma observations around Mercury.  
 However, in a future work such a density profile should be evaluated and included. A good opportunity would be to use the  
 plasma data from the recently launched two spacecraft mission BepiColombo, where the Mercury Magnetospheric Orbiter  
 (MMO also referred to as Mio) will probe Mercury's magnetosheath and solar wind with unprecedented fast measurements of  
 180 the particle distribution functions.

The model presented in this paper is generally robust and easy to implement. It can help to determine the local plasma  
 conditions of a spacecraft in the magnetosheath exclusively on basis of the upstream solar wind parameters.



185 *Code availability.* An IDL program to evaluate plasma flow velocity vector in Mercury's magnetosheath from solar wind parameters of the Tao solar wind propagation model can be retrieved from OSF: [https://osf.io/9jgqn/?view\\_only=2624aca3774c4ba8885dcb21a13e1b08](https://osf.io/9jgqn/?view_only=2624aca3774c4ba8885dcb21a13e1b08) (Schmid, 2020).

*Data availability.* The plasma data of the heliospheric Tao model are open access and can be retrieved on the AMDA website (<http://amda.cdpp.eu/>, Centre de Données de la Physique des Plasmas (CDPP), 2018) via the WorkSpace Explorer: DataBase/Solar Wind Propagation Models/Tao Model/SW Input OMNI (Tao *et al.*, 2005). The orbital motion data of Mercury are provided by the Navigation and Ancillary Information Facility (NAIF) and can be retrieved on the NAIF website under <https://wgc.jpl.nasa.gov:8443/webgeocalc> (Acton, 1996).

190 *Author contributions.* DS initiated this study, collected the data and implemented the method. FP, YN, MV and WB helped evaluating the manuscript.

*Competing interests.* The authors declare that they have no conflict of interest.

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