Long Range Plasma Momentum Coupling by High Voltage Static Electric field and Deep Space Exploration

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- 6 **Abstract.** Space exploration has been long constrained by the efficiency and capability of modern chemical rocket. Propellant-
- 7 less propulsion has been proposed as a solution to expand the boundary of space exploration. In this paper, we examine the
- 8 possibilities of a propellantless propulsion scheme through the interaction between the spacecraft and ambient plasma. The
- 9 spacecraft is charged to high electric potential by constantly shooting electrons away. The high voltage spacecraft will deplete
- the surrounding electrons, thus interact with a wide range of the background plasma (solar wind) and thus effectively extract
- 11 momentum from the plasma. By taking advantage of the exploitable ambient plasma, a spacecraft can reach very high speed,
- thus considerably reducing the travel time. The scheme is also applicable for braking, which is helpful in the exploration of
- inner planets like Venus and Mercury, and the stopping at the destination planets or stars.

1 Introduction

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Space exploration is the next step of human development. The main difficulty experienced in space travel is the long distance across planets, stars, or galaxies, and the low limitation of fuel. The average distance between planets in solar system is about 5.5 Astronomical units (AU) or 800 million km away, and the closest star system, the Alpha Centauri is 4.37 light-years (4.1 \times 10¹⁶m) away from solar system. Contemporary spacecraft can hardly reach a speed of 40 kms⁻¹, with the help of multiple slingshot acceleration of the planets. The speed is far too low, considering the travelling to the Alpha Centauri will takes longer than the entire human history.

Propellantless propulsion is a scheme proposed to overcome the problems of limited fuels carried by chemical rockets as well as ion thrusters. To date, various kinds of propellantless schemes such as electric sail and solar sail has been proposed as an alternative to chemical rockets for interplanetary or interstellar space travelling. In this paper, we propose a propellantless propulsion scheme by coupling the spacecraft with the ambient plasma to extract its momentum. The spacecraft is charged to high electric potential by constantly shooting electrons far away. The high voltage spacecraft will interact with a wide range of the background plasma (solar wind) in momentum and gain thrust. Comparing with the electric sail proposed by P. Janhunen (2007, 2014), the effective radius of the spacecraft can be held within 100 m to provide better control and manoeuvring.

The key challenge in the engineering for this scheme is maintaining high potential of the spacecraft. The spacecraft has to accelerate and shot electrons far away to remain high potential and couple with ambient plasma. As electron is the lightest charged particle, with a mass three orders of magnitudes smaller than the lightest ion, hence can be easily deflected by

magnets, electron acceleration is the easiest and most durable in engineering. Conventional non-superconducting electron injectors (Bluem et al. 2004) can accelerate electrons to 5 MeV with a compact size, and operate continuously at a maximum current of 1 A. These two parameters set an upper limit on the potential and current of our scheme.

The feasibility of maintaining high potential also limited by the field ion evaporation effect or field evaporation (FEV) (Zurlev et al. 2003). FEV is the removal of surface atom from its own lattice structure by induced electric field. The whole process is rather complicated and not well studied yet. In general, when the electric field of a surface exceeded certain threshold, called E^e , there will be significant increase in the FEV process and deplete the structure. A theoretical estimation given by Dinko N. Zurlev (Forbes, 2006) showed that the E^e for most metals is at the order of 10 Vnm⁻¹. For our spacecraft design with an effective radius of 100m, the threshold potential is at the order of 10^{12} V, which is 6 orders of magnitude beyond our limit and thus should not be a problem.

2 Concept

The spacecraft interact with the ambient plasma through static electric field. Comparing with the electric sail design as proposed by P. Janhunen, our concept consists of a spacecraft located at the centre and linked to several positively charged lightweight balls by conducting tethers. The distance from spacecraft to the balls could be a few hundreds of meters. The spherical shape of balls is designed to reduce the FEV effect. Due to electric static repulsion; all the balls will distribute evenly around the spacecraft. When deployed for operation, the electron gun is pointed to the opposite or perpendicular direction of the solar wind for ejecting the electrons away from the spacecraft. The whole structure can be treated as a metallic ball with an effective radius and a constant potential (being a conductor). As the potential profile outside the ball is close to Coulomb potential as explained below, the larger the effective radius is, the lower energy is required to shot the electrons away, hence the higher energy efficiency. The dynamic positively charged spacecraft-plasma combo can interact with much larger range of ambient plasma than in a quasi-neutral plasma as originally proposed by P. Janhunen, in which the influence of the potential is limited by Debye length.

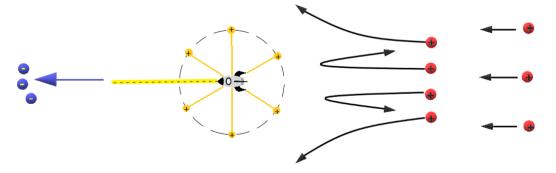


Figure 1: plasma wind coming from the right side being deflection by the electrostatic field of the spacecraft. The whole structure is consisted of a main unit at the center and connected to charged balls attached to the main unit.

For the sake of simplicity in simulation, the whole structure is treated as a sphere with the distance from spacecraft to the balls as the radius of the imaginary sphere. The sphere is charged to a surface potential of V_0 , A stream of plasma (solar wind) moving from the positive x direction. We consider only 1 species of ion, the protons. The deflection of protons from its trajectories provides the momentum. The loss in x-direction momentum of protons is transferred to the spacecraft. To calculate the trajectory and hence the momentum, the potential generated by the sphere need to be addressed. For theoretical estimation, we consider the potential to be a central force and takes the forms of either Coulomb potential or Debye potential.

In the absence of plasma, the potential generated by the sphere would be a simple Coulomb potential:

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$$V(r) = \frac{V_0 r_0}{r},$$
 (1)

- Where r_0 is the radius of the sphere and V_0 is the potential at the surface of the sphere and the potential at far point is zero.
- Due to the presence of ambient plasma, shielding occurred and the potential dropped by and exponential factor. The effective
- 66 potential is:

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$$V(r) = \frac{V_0 r_0}{r} e^{-\frac{r - r_0}{\lambda_D}},$$
 (2)

- Where λ_D is the effective Debye length, $\lambda_D = \sqrt{\varepsilon_0 (V_0 V_1)/n_0 e}$ (Janhunen et al. 2016). V_1 is the kinetic energy of the
- 69 incoming proton.
- We can estimate thrust by solving the equation of motion of the proton in a Coulomb potential. The deflection or
- 71 scattering of protons, θ from its original direction is calculated from:

$$72 b = \frac{V_0 r_0 e}{2E_k} \cot \frac{\theta}{2}, (3)$$

- Where b is the impact parameter, E_k is the kinetic energy of protons in solar wind. In this case, we set θ to 90 degree, the
- impact parameter b represent how far the electric field can affect and repel the protons from solar wind. Assuming $V_0 = 1$ MV,
- 75 $r_0 = 100 \text{ m}, E_k = 1.5 \text{ keV}, \text{ we can have the impact parameter } b = 33 \text{ km} \text{ and thus an effective scattering cross section of } constant the second section of the second section section of the second section section section of the second section se$
- 76 3400 km². The solar wind pressure at 1 AU from the Sun is 2 nPa and the spacecraft is estimated to acquire 6.8 N of thrust at
- the Earth's orbit.
- In reality, the potential can never be a symmetric Coulomb potential due to the presence of plasma. The next part of this paper will provide simulation result for the actual thrust obtained by the spacecraft.

3 1D Simulation

- 81 In 1D simulation, the system will reach a static condition after the spacecraft is charged. The particles (ions) interact with the
- 82 charged spacecraft and eventually the potential around the spacecraft takes the form as described by equation 2. The deflection
- 83 of protons from its own trajectory contribute the x-direction momentum to the spacecraft. As shown in figure 2, the spacecraft
- 84 is located at the origin. The ions is coming from the +x direction and assumed to have initial velocity in the x-direction. The
- 85 motion of the particle calculated by Runge-Kutta method with adaptive time-steps for error control.

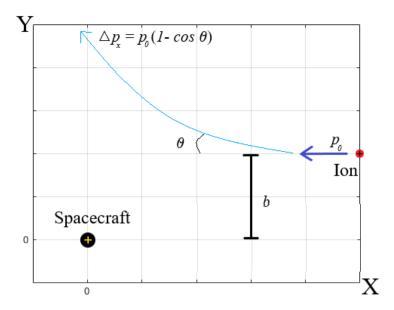


Figure 2: The spacecraft located at the origin and the ions from solar wind coming from the positive x direction.

The model for 1D simulation is rather simple. It provides the relation between the thrust generated and key parameters like spacecraft surface potential V_0 , radius r_0 and solar wind density n_0 . This provide a basis for calculating the trajectories for interplanetary travel for our spacecraft. Figure 3 and table 1 shows the scaling relation between the thrust and surface potential of surface as well as solar wind density.

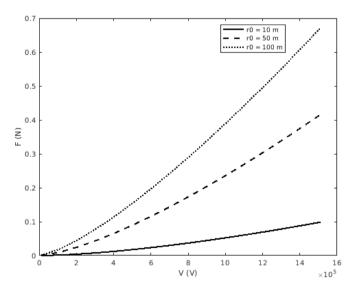


Figure 3(a): The relation between thrust F and the surface potential of the sphere V_0 . Dotted line: $r_0 = 100$ m, dashed line: $r_0 = 50$ m, solid line: $r_0 = 10$ m. Plasma density $n_0 = 1.2 \times 10^6$ m⁻³.

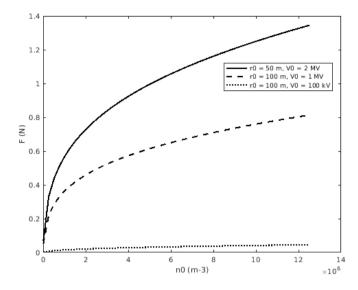


Figure 3(b): Figure 3(b) The relation between thrust F and the plasma density of solar wind n_0 . Dotted: $r_0 = 50$ m, $V_0 = 2$ MV, dashed: $r_0 = 100$ m, $V_0 = 1$ MV, solid: $r_0 = 100$ m, $V_0 = 100$ kV.

Table1: scaling relation between thrust F and V_0 , n_0 , r_0 .

$n_0/~10^5~{ m m}^{-3}$	V_0 / V	r_0 / m	Scaling
5.0	-	10	$F \propto V_0^{1.4715}$
5.0	-	50	$F \propto V_0^{1.3257}$
5.0	-	100	$F \propto V_0^{1.2771}$
1.0	-	100	$F \propto V_0^{1.3290}$
-	100 k	10	$F \propto n_0^{0.5723}$
-	100 k	100	$F \propto n_0^{0.4360}$
=	1.0 M	10	$F \propto n_0^{0.5330}$
-	1.0 M	50	$F \propto n_0^{0.3724}$
-	1.0 M	100	$F \propto n_0^{0.3183}$
5.0	100 k	-	$F \propto r_0^{0.8603}$
1.0	1.0 M	-	$F \propto r_0^{0.6804}$
5.0	1.0 M	-	$F \propto r_0^{0.6804}$

To estimate the electrons flux, we use the Orbital Motion Limited (OML) theory [1][10]. An electron will be captured when its trajectory meets the surface of the sphere. The electrons from solar wind coming from 1 direction, if the impact parameter (distance of electron from centre of sphere and perpendicular to its own velocity) lies within certain value, the electron will be absorbed by the sphere. Assuming that the electrons only come from solar wind, and experience a central force. With simple mechanic invariants, we can calculate the current:

$$I = \pi r_{\rm s}^2 e n_0 v, \tag{4}$$

108 Where n_0 is the density of the electron in solar wind, v is the velocity of incoming electron. $r_s = r_0 \sqrt{1 + \frac{2eV_0}{mv^2}}$ is the impact parameter. All electrons aimed at impact parameter less than r_s will hit on the surface of the sphere.

4 2D Simulation

In this section, we provide a PIC 2D simulation describe the behavior of the particles. The simulation region is has a cylindrical symmetry along the x-axis. Similar to figure 2, both the protons and electrons constantly flow in from the +x direction. The electric field is solved by Coulomb equation. The potential of the sphere (spacecraft) is V_0 . All the electrons moving inside the sphere are absorbed.

The simulation span across a region of 18 km * 9 km, with spatial grid varying linearly from 10 m to 1800 m. The grid size is small at the origin to provide a more precise result around the spacecraft. With plasma density of $n_0=5.0\times10^4~\rm m^{-3}$, the Langmuir frequency for electron is equivalent to $\omega_{pe}=1.3\times10^4~\rm s^{-1}$. The timestep is set to $\Delta t=7.75\times10^{-5}~\rm s$. We run 2 cases, (1) $V_0=1~\rm MV$, $v_0=100~\rm m$, (2) $v_0=2~\rm MV$, $v_0=50~\rm m$, with $v_0=1000~\rm m$.

Figure 4(a) shows the established stable contour plot of the potential. The horizontal axis (X-axis) is parallel to the direction of solar wind (coming from right). We can see there is a high potential area on the incoming side of the solar wind. This means the spacecraft can couple or interact with a large range of the ambient plasma. Figure 4(b) is for ion density. The concentration of ions on the right side is because the ions have nowhere to go. Figure 4(c) is for electron density; note the high concentration of electrons around the spacecraft.

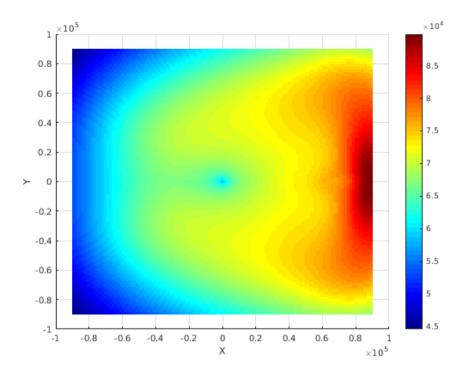
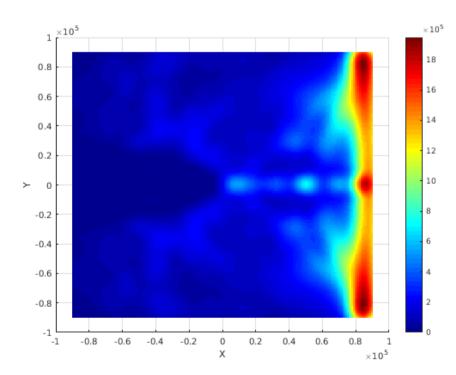


Figure 4(a): The plasma potential when simulation reached static state ($T=32000~\Delta t, \Delta t=7.75\times10^{-5}~s$), the spacecraft located at the origin.



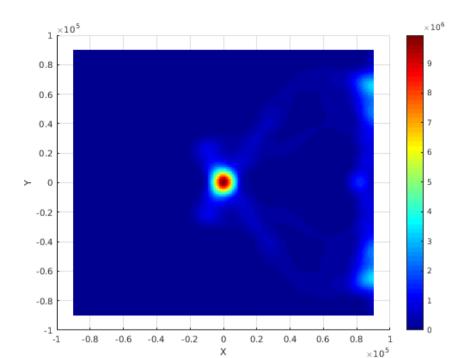


Figure 4(c): The electron density when simulation reached static state. Electrons in the region almost depleted.

The thrust acting on the sphere and the electron current is calculated and compared with 1D simulation in table 2. In 2D simulation, the thrust is 2~3 times larger than that of 1D simulation, and the electron current lower. As 1D simulation is based on plasma shielding, hence, larger thrust in 2D simulation imply the momentum coupling between the spacecraft and the ambient plasma is stronger than plasma shielding.

Table 2: Comparison between 1D and 2D simulation result.

	V_0 , r_0	1D Si	mulation	2D Simulation		
		Thrust / N	Current / mA	Thrust / N	Current / mA	
_	1 MV, 100 m	0.52	168	1.6	102	
	2 MV, 50 m	0.77	84	1.6	73	

5 Interplanetary Travel

In this section, we consider a simplified journey starting from Earth's orbit to outer planet such as Mars and Jupiter. Id calculation only takes account of single particle trajectory, other than the collective behavior of the plasma, the result may serve as a reference, and 2D simulation can estimate the thrust generated by solar wind. The thrust generated depends on the ambient plasma density n_0 , and n_0 drops by inversely square law of the distance, D, from the Sun.

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$$F(D) = A \cdot D^k,\tag{5}$$

Where F is the thrust, D is the distance to the Sun. k is a scaling coefficient obtained from 1D simulation. A is a constant determined by 2D simulation. From 1D simulation, k is within the range from -1.3 to -1.5 (due to the fact that distance to the Sun affect the plasma density and plasma shielding effect). Adding the force into the equation of motion of the spacecraft:

$$m(\ddot{D} - D\dot{\theta}^2) = -\frac{GM_Sm}{D^2} + F(D),\tag{6}$$

Where M_S and m are the mass of the Sun and spacecraft respectively, θ is the angular coordinate of the spacecraft in a polar coordinate system with the Sun located at the center. By solving the equation of motion numerically with initial distance being the radius of the orbit of the Earth, radial velocity being zero and tangential velocity equal to that of Earth, we can calculate the trajectories of the spacecraft. Table 3 shows the time taken for each mission under various circumstances. The main power consumption is from the electron accelerator (gun). It is calculated by multiplying the current of the electron gun and the potential of the spacecraft.

Table 3: Time taken for spacecraft to a journey to reach different planets.

			Initial		Time taken (days)		Power	
V_0	r_0	m	acceleration					
(MV)	(m)	(kg)	(mms ⁻²)	Mars	Jupiter	Saturn	Pluto	(kW)
0.3	100	240	0.85	265	-	-	-	10
0.5	100	200	2.0	115	473	745	7.5 years	26
0.5	100	300	1.3	152	834	1308	12 years	26
1.0	50	300	2.0	113	473	756	8 years	18
1.0	50	500	1.2	164	1206	1903	16 years	18

The most efficient way for sending spacecraft to a target planet is by orbit transfer (Janhunen et al. 2014). The spacecraft is transfer from a smaller orbit (Earth) to a larger orbit (Mars) following a Hohmann transfer orbit. In our case, for planets like the Mars, the spacecraft can follow a similar orbit for energy efficiency. With a surface potential $V_0 = 0.3$ MV, effective radius $r_0 = 100$ m, a spacecraft of mass m = 240 kg can be transferred to the Mars.

6 Result and discussions

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We proposed an ambient plasma momentum coupling spacecraft propelling scheme by utilizing high electric potential for the spacecraft to interact with a wide range of background plasma, which can be considered as a compact electric sail with a much smaller structure.

Preliminary calculations show that it is promising in space exploration. The simulation result shows that with a surface potential of the spacecraft of 1 MV, this scheme can produce a thrust of about 0.6 N, by consuming a power of about 18 kW. The simulation is performed in low plasma density. Since this scheme requires no propellant, it has an advantage over chemical rockets and ion thrusters. Comparing with the E-sail proposed by P. Janhunen, the relatively smaller structure (100 m to 1km versus 10 km) should be much easier to control or manoeuver. A simple calculation shows that a spacecraft of 500 kg can reach Mars in 164 days and Pluto in 16 years.

The scheme is also applicable in braking, as long as the momentum of ambient plasma is exploitable. In situations like braking near Jupiter, travelling to the inner planets, the plasma trapped by Jupiter and the solar wind can be used for braking.

This scheme can achieve very high interstellar travelling speed by delivering artificial dense and energetic beams to the spacecraft over a very long distance, by, for example, a series of powerful particle accelerators on the Moon, other satellites, or dwarf planets, thus drastically shorten the travelling time to the nearest stars from tens of thousands of years to a few hundreds of years.

If the situation is favorable, such as in a cosmic jet, a spacecraft could be accelerated to relativistic velocities.

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