



Evaluation of the IGS-Global Ionospheric Mapping model over Egypt

Mostafa RABAH¹, Ahmed Sedeek²

¹: Civil Eng. Dpt., Benha Faculty of Engineering, Benha University, Egypt.,

*Correspondence: mrabah@bhit.bu.edu.eg

²: Civil Eng. Dept., Higher Institute of Engineering and Technology - Bihira, Egypt

Abstract:

Global ionosphere maps (GIM) are generated on a daily basis at CODE using data from about 400 GPS/GLONASS sites of the IGS and other institutions. The vertical total electron content (VTEC) is modeled in a solar-geomagnetic reference frame using a Spherical Harmonics Expansion “SHE” up to degree and order 15. To cover the holes of the first GIM computation stage existing in the North Africa and over the Oceans resulting a shortage of GNSS station in North Africa, an optimum spatial-temporal interpolation technique was developed to cover these holes (Krankowski and Hernandez-Pajares, 2016).

The current paper evaluates the ionospheric correction by Global Ionospheric Maps, GIM, provided in (IONEX) files produced by International GNSS Services “IGS”. The evaluation is performed based on investigating the effect of a given GIM ionospheric correction on kinematic relative positioning solutions. The evaluation was done using several baselines of different lengths in Egypt. The results show that there is no significant effect of the provided GIM values on the solution of kinematic processing. The results confirm that although there is a lack of International GNSS Service (IGS stations) over North Africa, GIMs have no effect in mitigating ionospheric error. A new value for the ionosphere correction VTEC values was obtained by a regional, developed algorithm based on zero-differenced phase ionospheric delay (ZDPID) (Tawfeek et.al., 2018). These new values of VTEC were fed into GIMs for the specified stations data. A useful result was obtained for correcting the ionospheric error over kinematic solution of many baseline lengths up to 300 km which demonstrates validity of the proposed evaluation method.

Key words: International GNSS Services “IGS”, Global ionospheric maps “GIM”, vertical total electron content (VTEC), Zero-differenced phase ionospheric delay

1. Introduction

Global ionosphere maps (GIM) are generated on a daily basis at CODE using data from about 400 GPS/GLONASS sites of the IGS and other institutions, see figure (1). The vertical total electron



content (VTEC) is modeled in a solar-geomagnetic reference frame using a Spherical Harmonics Expansion “SHE” up to degree and order 15. Piece-wise linear functions are used for representation in the time domain. The time spacing of their vertices is 2 hours, conforming with the epochs of the VTEC maps. Instrument biases, so-called differential P1-P2 code biases (DCB), for all GPS satellites and ground stations are estimated as constant values for each day, simultaneously with the 3328 parameters used to represent the global VTEC distribution. The DCB datum is defined by a zero-mean condition imposed on the satellite bias estimates. P1-C1 bias corrections are taken into account if needed. To convert line-of-sight TEC into vertical TEC, a modified single-layer model (MSLM) mapping function approximating the JPL extended slab model mapping function is adopted. The global coverage of the GPS tracking ground stations considered at CODE is shown in figure (1).

According to Hernández-Pajares et al. (2017), broadly used Global Ionosphere Maps (GIMs) provided by the IGS are characterized by estimated accuracy ranging from a few TECU to approximately 10 TECU in VTEC. This IGS product offers 2.5 by 5.0 degrees spatial resolution, and temporal resolution of 2 h. IGS GIMs are developed as an official product of the IGS Ionosphere Working Group by performing a weighted mean of the various Analysis Centers (AC) VTEC maps: CODE, ESA, JPL, UPC, and NRCan. CODE GIM (CODG) comes from processing double-differenced carrier phase data and TEC parametrization using Spherical Harmonics Expansion “SHE” functions and Bernese software (Schaer, 1999). ESA GIM is based on processing carrier phase-smoothed pseudoranges and TEC parametrization using SHE functions (Feltens, 2003). JPL GIM is derived from a three-shell model that is based on spline functions.

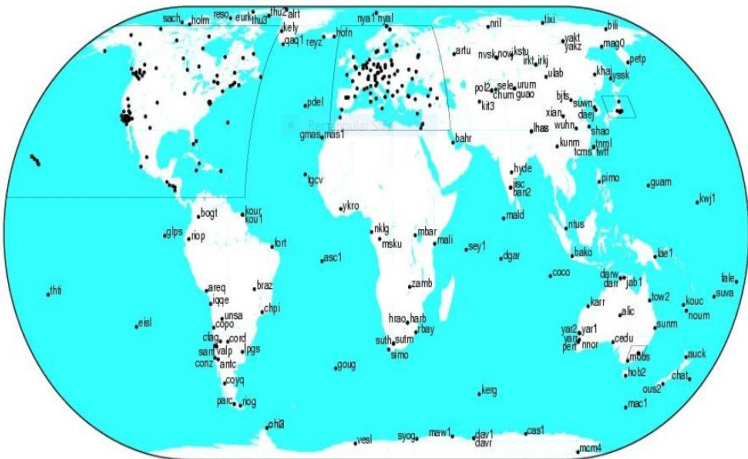




Figure (1): IGS directly manages ~400 permanent GNSS stations observing 4-12 satellites at 30 s 52
 rate: more than 250,000 STEC observations/hour worldwide, but there is lack of stations in some 53
 areas (e.g., over the oceans). 54

According to Hernández-Pajares et al. (2009), the highest accuracy is offered by the UQRG model 55
 provided by UPC, and is produced by combining a tomographic modelling of the ionosphere with 56
 kriging interpolation using the TOMION software developed at UPC. UQRG offers 2.5 by 5.0 57
 degrees spatial resolution, and high temporal resolution of 15 min (Orús et al., 2005). It should also 58
 be noted that vertical TEC values estimated by using smoothed pseudoranges have lower accuracy 59
 than values offered by methods based on the precise carrier phase observations. 60

The majority of various global and regional ionosphere models currently available are characterized 61
 by low temporal and spatial resolutions. Most of them are based on carrier phase-smoothed 62
 pseudorange data, which presents low accuracy and requires strong smoothing filters. As a result, the 63
 obtained ionospheric delay represents relatively low accuracy of several TEC units (1 Total Electron 64
 Content Unit = 1 TECU = 10^{16} el/m², and it is equivalent to 0.162 m of L1 signal delay). This is one 65
 of the reasons why spherical harmonics expansion (SHE) is used for the global and regional TEC 66
 parameterization (Rovira-Garcia, 2017). The smoothing effect of SHE undoubtedly results in the low 67
 accuracy of the ionospheric models. Also, the ionosphere models often use GPS-only data. Another 68
 important aspect is using a single layer model (SLM) ionosphere approximation and its associated 69
 relatively simple mapping function, which results in a rather low relative accuracy of publically 70
 available models that amounts to 20–30%, as was shown in Hernández-Pajares et al. (2011). 71

Precise kinematic positioning to centimeter level accuracy requires using the carrier phase 72
 observations with the correct resolution of the integer ambiguities. Conclusions previously published 73
 for solving the ambiguities of medium baselines On-The-Fly can be summarized in the following 74
 two different approaches (El-Hattab et al., 2003): 75

1. The main layout of the first approach can be represented by the following two steps: The first 76
 step is a static initialization for the rover receiver at the beginning of the mission within a short 77
 distance with respect to a reference receiver. This will facilitate the processing of the ambiguity 78
 fixing. In the second step, a technique for ambiguity recovery On-The-Fly is introduced to 79
 recover the integer ambiguities when cycle slips or data gaps shorter than a few minutes occur. 80
2. The second approach mainly depends on the condition that the dominant source of distance- 81
 dependent errors is the ionospheric refraction compared to the orbit error as well as the 82
 tropospheric error. As is known, the tropospheric error is mostly affected by the height difference 83



between the ends of the baseline rather than the distance. Hence, the ionospheric error produces
 the dominant contribution in complicating the ambiguity resolution of a medium baseline
 compared to the other errors. Therefore, providing a proven correct ionospheric correction to the
 processing will enhance the ambiguity resolution process.

The current study evaluates the possibility of using Global Ionospheric Maps for mitigating
 ionosphere effect (large error source) over Egypt. The evaluation process is undertaken by
 incorporating the derived GIM-VTEC values into the processing of baselines different lengths (up to
 300 km) in kinematic mode to check how the processing results are improved. Finally, the analysis
 of the obtained results and graphs supported with the statistical analysis is discussed and presented,
 from which the important conclusions and recommendations are drawn.

2 Methodology

2.1 GPS Observation equations

The observation equations for code and carrier phase measurements on the L_i frequency ($i = 1, 2$) can
 be formulated as follows (Hoffmann et al., 2013):

$$P(L_i) = \rho + c(dt - dT) + d_{orb} + d_{trop} + d_{ion/li} + d_{mult(P_{li})} + \epsilon(P_{li}) \quad (1)$$

$$\varphi(L_i) = \rho + c(dt - dT) + d_{orb} + d_{trop} + d_{ion/li} + \lambda_i N_i + \lambda_i (\varphi_r(to, li) - \varphi_s(to, li)) + d_{mult(\varphi_{li})} + \epsilon(\varphi_{li}) \quad (2)$$

Where:

| | | |
|----------------|--|--|
| $P(L_i)$ | : Measured pseudo range on L_i (m). | |
| $\varphi(L_i)$ | : Measured carrier phase on L_i (m). | |
| ρ | : True geometric range (m). | |
| c | : Speed of light (m/s). | |
| dt | : Satellite clock error (s). | |
| dT | : Receiver clock error (s). | |
| d_{orb} | : Satellite orbital error (m). | |
| d_{trop} | : Tropospheric delay (m). | |
| $d_{ion/li}$ | : Ionospheric delay on L_i (m). | |
| λ_i | : Wavelength (m). | |
| N_i | : Integer ambiguity on L_i (cycle). | |



| | | |
|--------------------------|---|-----|
| $\varphi_r(to, li)$ | : Initial phase of receiver oscillator. | 113 |
| $\varphi_s(to, li)$ | : Initial phase of satellite oscillator. | 114 |
| $d_{mult}(P_{li})$ | : Multipath effect in measured pseudo range on Li (m). | 115 |
| $d_{mult}(\varphi_{li})$ | : Multipath effect in measured carrier phase on Li (m). | 116 |
| $\epsilon(P_{li})$ | : Measurement noise (m). | 117 |

Denoting the stations by a and b and the satellites involved by j, k, the double difference model for long baselines when there is a significant difference in the atmospheric effect between the two baselines ends and elevation angles at both stations are different can be expressed:

$$\begin{aligned} \nabla\Delta\varphi_{ab}^{jk}(t) = & \rho_a^j(t) - \rho_a^k(t) - \rho_b^j(t) + \rho_b^k(t) + \lambda\nabla\Delta N_{ab}^{jk}(t) + \nabla\Delta dorb_{ab}^{jk}(t) + \nabla\Delta dtrop_{ab}^{jk}(t) \\ & - \nabla\Delta dion_{ab}^{jk}(t) + \nabla\Delta dmult_{ab}^{jk}(t) + \nabla\Delta\epsilon_{ab}^{jk}(t) \end{aligned} \quad (3)$$

The term $\nabla\Delta N_{ab}^{jk}(t)$ is called the double difference integer ambiguity, that must be determined (as an integer) during the double difference carrier phase processing procedure. If the individual carrier phase observations are continuously made over time (no cycle slip), the integer ambiguity terms remain constant. If these terms can be successfully determined to integer values, the fixed solution to the baseline is achievable. In the case of short base lines, the residual orbital errors ($\nabla\Delta dorb_{ab}^{jk}(t)$), residual ionospheric errors ($\nabla\Delta dion_{ab}^{jk}(t)$), and residual tropospheric errors ($\nabla\Delta dtrop_{ab}^{jk}(t)$) can be considered negligible (Hofmann, 2008). Multipath errors are not mitigated by differencing observations, and hence a user should try to avoid multipath environments whenever possible as the best approach to mitigating their effects (Abu Galala et al., 2018).

For medium and long baselines common error does not cancelled out. Because of different elevation angles on both ends of baseline there is no correlation between the errors. Using precise orbit and clock products with centimeter level accuracy, the two errors related with the broadcast orbits and clocks can be significantly reduced. Satellite and receiver clock error does not depend on baseline length, so it can be cancelled by differencing. For the tropospheric residual errors, the best standard method of computing is to apply a tropospheric error model at the locations of the reference and remote stations. Examples of such models include the Hopfield model and the Saastamoinen model (Hoffman, 2008).

2.2 Ionospheric modelling



The ionospheric delay has an intensive impact on the GNSS observations by driving an additional transmission time delay. The magnitude of this effect is determined by the amount of total electron content (TEC) and the frequency of signal. Under normal solar activity conditions, this effect on GPS signals is usually in the range from a few meters to tens of meters, but it can reach more than 100 m during severe ionosphere storms (Rovira-Garcia, 2015). TEC is quantified from GPS measurements by a linear combination of the measured pseudo range and phase observables registered by the receiver on two carrier frequencies ($f_1 = 1575.4$ MHz and $f_2 = 1227.6$ MHz). TEC is measured in TECU units with $1 \text{ TECU} = 10^{16} \text{ el/m}^2$.

The geometry-free linear combination of GPS observations is used for ionospheric estimation and it is obtained by subtracting simultaneous pseudo range ($P_1 - P_2$ or $C_1 - P_2$) or carrier phase observations ($\varphi_1 - \varphi_2$). Code-based TEC (TEC_P) is noisier than phase-based TEC (TEC_φ), largely due to multipath, but the phase-based suffers an unknown integer ambiguity offset and is subject to cycle slips associated with rapid ionospheric scintillations. The resultant TEC is the GPS-derived slant TEC along the signal path between satellite and receiver (Zus et al., 2017). In this combination, the satellite – receiver geometrical range and all frequency independent biases are removed. The geometry-free linear combination for carrier phase observations is obtained:

$$L_4(t) = \varphi_{GF} = \varphi_1 - \varphi_2 = (\gamma - 1)dion_1 + \lambda_1 N_1 - \lambda_2 N_2 + \varepsilon(\varphi_1 - \varphi_2) \quad (4)$$

Where: $\varepsilon(\varphi_1 - \varphi_2)$ is the noise term in phase equation can be neglected for simplicity, the factor γ is the factor to convert the ionospheric delay from L2 to L1 frequency.

$$dion_2 = \frac{40.3 \text{ STEC}}{f_2^2} = \frac{f_1^2}{f_2^2} Dion_1 = \gamma Dion_1 \quad \gamma = \frac{f_1^2}{f_2^2} \quad (5)$$

2.3 VTEC Estimation

The ionosphere may be considered as a thin single layer surrounding the earth at a fixed height from the earth for which all free electrons in the ionosphere are assumed to be concentrated, in this single-layer having a maximum electron density (10^{11} – 10^{12} e/m^2 around 300–500 km) (Feltens, 2003). IPP is the intersection point between the satellite receiver line-of-sight, and the ionosphere shell (Figure 2). Slant total electron content (STEC) can be translated into VTEC using Single Layer Model (SLM).

$$VTEC = F(E) \text{ STEC}$$



$$VTEC = F(E) \frac{dion_1 \cdot f_1^2}{40.3}$$

Where: $F(E)$ is the mapping function.

Mapping function model:

To compute elevation and azimuth angle for any satellite, the satellite position coordinate (x_s, y_s, z_s) in ECEF at the specified epoch is deduced from the IGS final orbits. The interpolated satellite position is then transformed to a local coordinate frame, East, North, and Up (ENU) system. The transferred ENU is used to calculate elevation and azimuth angles as follows (Sedeek et al., 2017):

$$E = \arctan\left(\frac{x_U}{\sqrt{x_N^2 + x_E^2}}\right) \quad A = \arctan\left(\frac{x_E}{x_N}\right)$$

Where: E and A are elevation angle and Azimuth angle of satellite at the receiver, respectively. The receiver position in Earth Centered Earth Fixed (ECEF) is converted to geodetic coordinates. Ionospheric Pierce Point (IPP) is the intersection point between the satellite and the receiver line-of-sight. Ionospheric Pierce Point (IPP) location can be computed by providing reference station coordinates (ϕ_r, λ_r) , from which the geographic latitude and longitude of IPP can be computed according to elevation and azimuth angle of satellite as follows (Sedeek et al., 2017):

$$\psi = \pi / 2 - E' - E$$

Where ψ : The offset between the IPP and the receiver; E' and E : the elevation angles of the satellite at the IPP and receiver.

$$E' = \sin^{-1}\left(\left(\frac{R_E}{R_E + H}\right) \cos E\right)$$

R_E : is the mean radius of the spherical Earth (6371 km)

H : is the height of IPP (taken to be 450 km)

$$\phi_{IPP} = \sin^{-1}(\sin(\phi_r) \cdot \cos(\psi) + \cos(\phi_r) \cdot \sin(\psi) \cdot \cos(A))$$

$$\lambda_{IPP} = \lambda_r + \frac{\psi \cdot \sin(A)}{\cos(\phi_{IPP})}$$



3. GIM Evaluation

To evaluate the obtained ionospheric TEC values that are produced by IGS, the IONEX data file for a specified time is imported. This data if used with GNSS data should improve the position solution and/or enhance ambiguity resolution of a specified baseline that cannot be fixed under normal conditions, otherwise the quality of the imported ionospheric data is not good enough to support the positioning works. However, our evaluation approach is built on applying the imported IONEX data on a third-party processing SW, Trimble Total Control, known as TTC, for collected baselines of different lengths. The processing is performed on a kinematic mode. Alternative ion TEC data, generated by regional model was applied to evaluate the validity of the proposed evaluation approach.

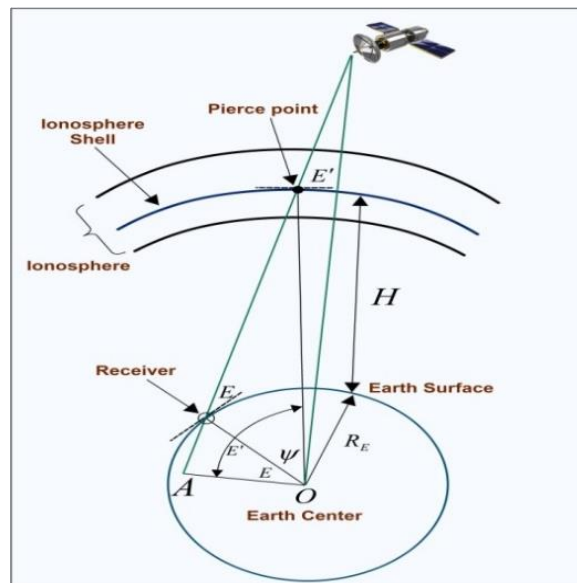


Figure (2): Elements of the spherical ionospheric shell model (Sedeek et al., 2017).

3.1 Data Description

The data used for the evaluation study, refer to figure (3), were collected on April 15, 2015 at seven stations: six of them, is the northern part of the Egyptian Permanent GNSS Network (EPGN) established by the National Research Institute of Astronomy and Geophysics NRIAG at 2006 and the seventh station in Alexandria managed by the French institute, Centre d'Études Alexandrines (CEALX). All NRIAG Stations are equipped with Trimble Net R5 Dual frequency GNSS receivers whilst Alexandria is equipped with a LEICA GRX1200 GG-Pro Dual frequency GNSS Receiver.



The data sample rate was 30 seconds epoch interval. The number of visible satellites varied between 224
 6 and 10 during the test period. As is shown in figure (3), all the used GNSS stations are located 225
 between Latitudes 30° & 32° and Longitudes 25° & 33°. 226

3.2 Processing Software 227

For baseline processing, Trimble Total Control 2.7 (TTC2.7) was the main processing software 228
 package that was used for the kinematic processing of the data. TTC has the capability to implement 229
 precise ephemeris and global ionospheric maps (IONEX). On the other hand, for Precise Point 230
 Positioning (PPP), the online service provided by Natural Resources Canada (NRCan) was utilized to 231
 provide the threshold values for comparison (Rabah et al., (2016). The **NRCan Online Precise Point** 232
Positioning Software is developed by NRCan to supply various users' application requirements. The 233
 PPP service can be used to process data collected by any single-or dual-frequency receiver, and the 234
 data can be observed in static or kinematic modes. PPP is accessible via the Internet by logging into 235
 the NRCan website (http://www.geod.nrcan.gc.ca/online_data_e.php). 236
 237

3.3 GIM data 238

Table (1) shows a part of the IONEX data that was assigned for the specified latitude location of first 239
 epoch of day April 15, 2015. The evaluation process is **carried** out by incorporating the derived GIM- 240
 VTEC values into the processing of different baseline lengths (up to 300 km), in kinematic mode and 241
 check how the processing results are improved. The evaluation was performed on several lengths of 242
 baselines, see table (2), and processed with TTC software, with and without IONEX in Kinematic 243
 mode. Unfortunately, the results show that the IONEX file did not affect the results at all: no 244
 differences were found in solutions with and without IONEX. The results confirm that there is no 245
 significant effect of the provided GIM values on the solution of kinematic processing. The results of 246
 GIM values forced us to check the validity of Ion TEC values in the IONEX file for the specified 247
 area. A trial was undertaken to compute alternative regional TEC values using another model. 248
 249

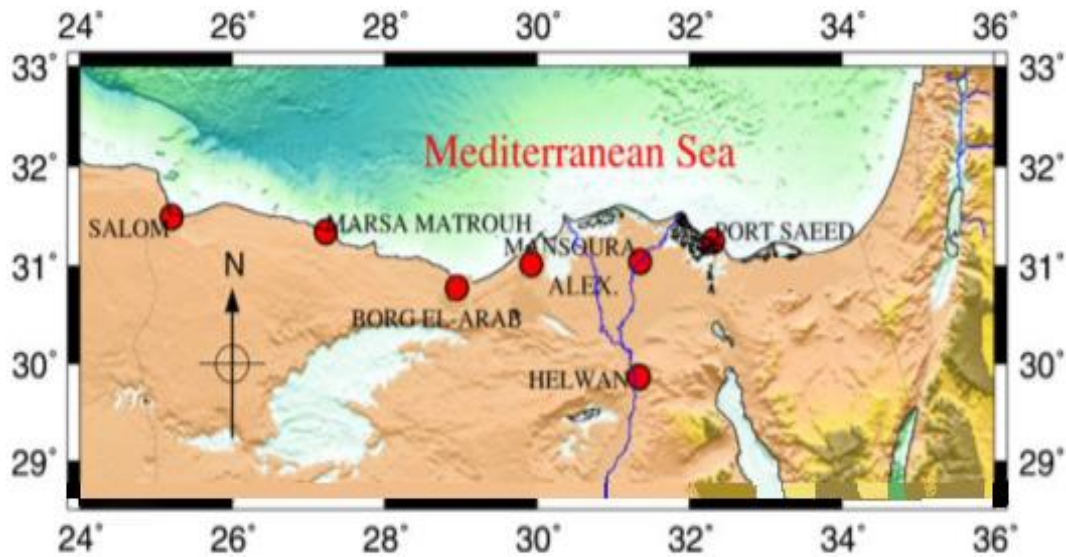


Figure (3): The location of the used stations

Table (1): Sample of the used IONEX file

| | | | | | | | | | | | | | | | | | | | | | | | | | |
|----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------------------|--|--|--|--|--|--|--|--|--|--|
| 2015 4 15 0 0 0 | | | | | | | | | | | | | | | EPOCH OF CURRENT MAP | | | | | | | | | | |
| 32.5-180.0 180.0 5.0 450.0 | | | | | | | | | | | | | | | LAT/LON1/LON2/DLON/H | | | | | | | | | | |
| 621 | 632 | 633 | 630 | 628 | 630 | 630 | 621 | 594 | 553 | 508 | 471 | 448 | 438 | 436 | 434 | | | | | | | | | | |
| 433 | 429 | 422 | 414 | 404 | 390 | 372 | 351 | 331 | 318 | 315 | 320 | 333 | 348 | 360 | 363 | | | | | | | | | | |
| 352 | 330 | 305 | 283 | 263 | 247 | 230 | 215 | 208 | 209 | 215 | 221 | 221 | 215 | 202 | 186 | | | | | | | | | | |
| 170 | 156 | 149 | 153 | 169 | 196 | 228 | 253 | 269 | 277 | 287 | 301 | 319 | 337 | 352 | 364 | | | | | | | | | | |
| 373 | 384 | 404 | 435 | 475 | 521 | 564 | 598 | 621 | | | | | | | | | | | | | | | | | |
| 30.0-180.0 180.0 5.0 450.0 | | | | | | | | | | | | | | | LAT/LON1/LON2/DLON/H | | | | | | | | | | |
| 657 | 668 | 669 | 664 | 660 | 659 | 657 | 648 | 623 | 585 | 542 | 507 | 485 | 474 | 469 | 466 | | | | | | | | | | |
| 461 | 456 | 449 | 439 | 424 | 404 | 378 | 351 | 330 | 321 | 328 | 347 | 376 | 406 | 430 | 438 | | | | | | | | | | |
| 425 | 396 | 361 | 330 | 304 | 280 | 256 | 233 | 218 | 213 | 216 | 220 | 221 | 214 | 202 | 187 | | | | | | | | | | |
| 173 | 161 | 154 | 158 | 174 | 201 | 231 | 256 | 270 | 277 | 285 | 300 | 320 | 341 | 360 | 374 | | | | | | | | | | |
| 385 | 397 | 419 | 453 | 497 | 546 | 593 | 631 | 657 | | | | | | | | | | | | | | | | | |

Table (2): The baseline used in verification

| Baseline | | |
|--------------------|-------------------|-------------|
| From | To | Length (Km) |
| Borg-Alarab (Borg) | Alexandria (Alex) | 49.05 |
| Port-Said (Said) | Mansura (Mnsr) | 94.47 |
| Helwan | Mansura (Mnsr) | 130.76 |
| Borg-Alarab (Borg) | Mansura (Mnsr) | 171.11 |



| | | |
|--------------------|--------------------|--------|
| Helwan | Port-Said (Said) | 179.51 |
| Helwan | Borg-Alarab (Borg) | 203.05 |
| Port-Said (Said) | Alexandria (Alex) | 229.05 |
| Borg-Alarab (Borg) | Port-Said (Said) | 264.98 |

A new algorithm based on Zero-differenced phase Ionospheric Delay (ZDPID) was developed (Tawfeek et.al., 2018). The core of this algorithm is mainly dependant on computing the TEC values by using carrier phase and GPS phase ambiguity resolution model by using Sequential Least Square Adjustment. The proposed algorithm has been written using MATLAB code. The TEC values are computed for the aforementioned stations every epoch, 30 sec., then an average TEC values were computed every two hours similar to the GIM in IONEX file. The TEC values of the ZDPID with IONEX-IGS are depicted in figure (4). As is shown in figure (4), the TEC differences between the regional ZDPID values and the IONEX-IGS values exceed several tens of TEC units especially in the early morning with reduced values given at noon.

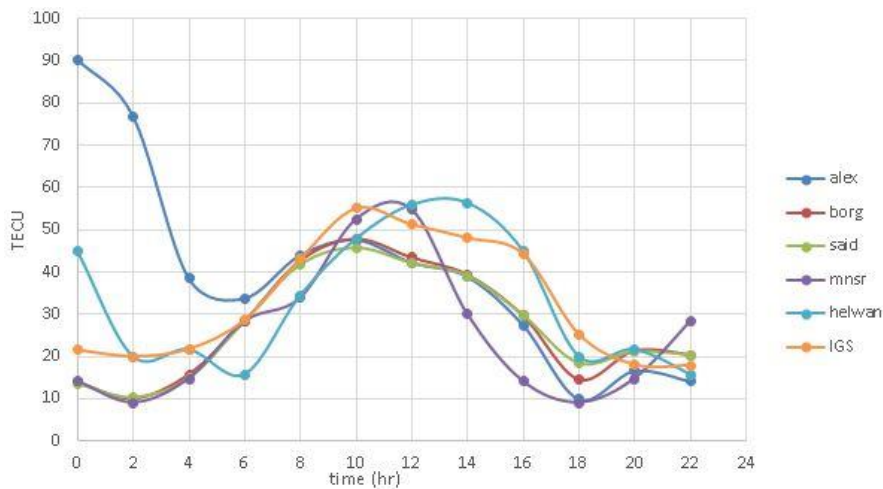


Figure (4): Mean TEC results every 2 hours of the study stations with comparison to IGS GIMs Day 105, 2015

Krankowski and Hernandez-Pajares (2016) confirmed that due to the shortage of GNSS stations in North Africa, the first GIM computation stage suffered from the hole existing in North Africa and over the Oceans, see figure (5). They deployed an optimum spatial-temporal interpolation technique to cover these holes. Based upon the above discussion, it is easy to confirm that the derived



ionospheric TEC values derived from IONEX GIM products are not feasible and useless for use in
precise positioning.

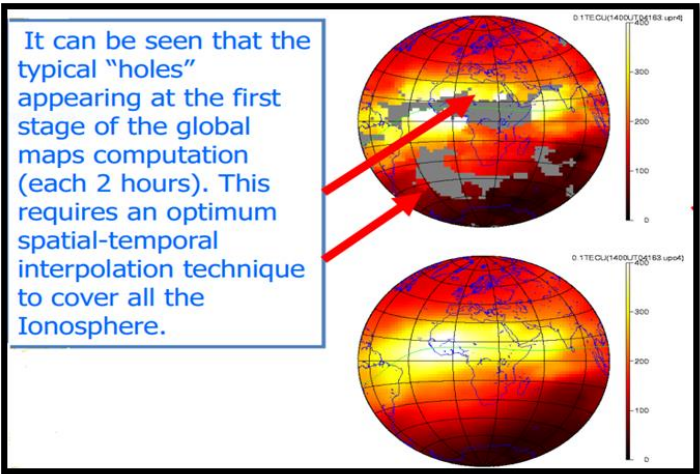


Figure (5): The holes of the GIM computation as indicated by (Krankowski and Hernandez-Pajares, 2016)

3.4 Modifying GIM-IONEX data

To modify the TEC data given in the IONEX file, the procedures described in the flow chart depicted in figure (6) were applied. Table (3) demonstrates a sample of the original TEC values as given in IONEX file and the modified values for Borg and Port Said stations at April 15, 2015. However, to see the validity of the computed regional Ionospheric TEC against the IONEX values, four baselines, namely Baseline Helwan ~ Mnsr 130.76 km, baseline Helwan ~ Said 179.51 km, baseline Helwan ~ Borg 203.16 km and baseline Borg ~ Said 264.98 km, were processed twice by TTC. The first processing was done without using any ionospheric correction and the second by using the modified IONEX files. The following chapter demonstrates the results of the processing of different baseline varying from 100 km to 270 km.

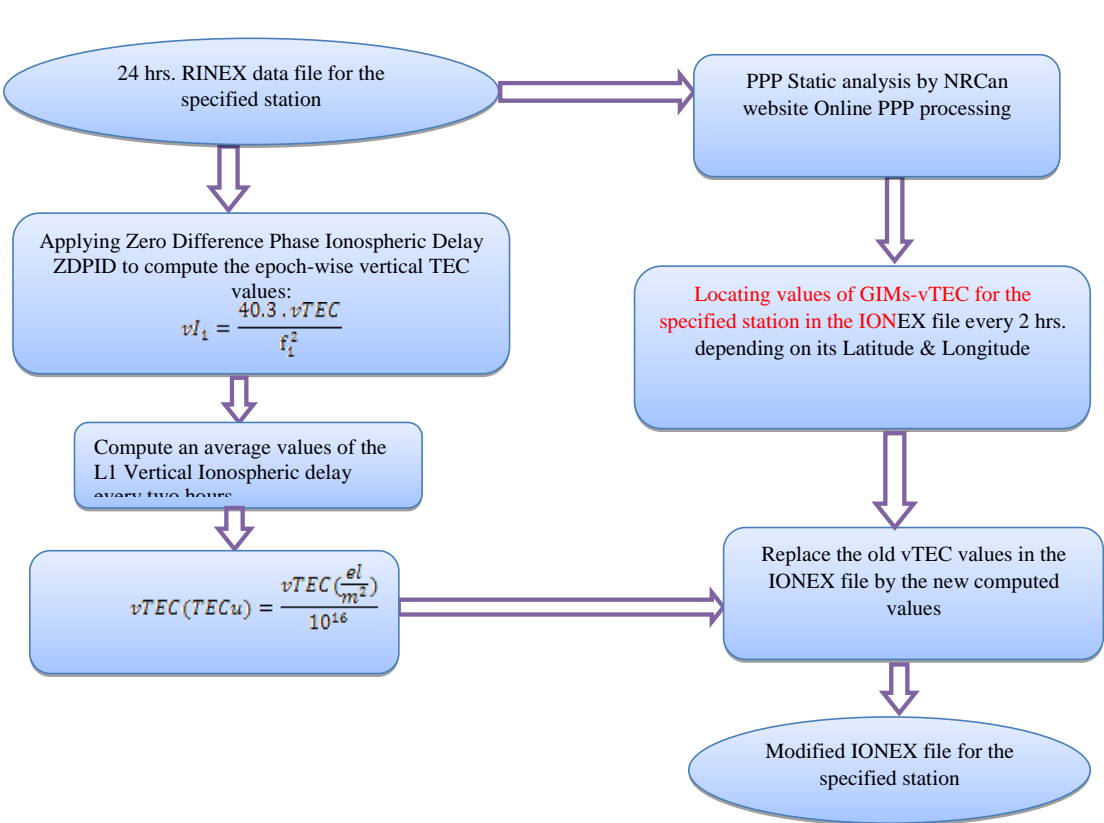


Figure (6): A description of the procedures that were used in modifying the VTEC values in the IONEX file.

Table (3): A sample Modified TEC values in IONEX file for the specified area in Egypt

| 32.5-180.0 180.0 5.0 450.0 | | | | | | | | | | | | | | | LAT/LON1/LON2/DLON/H | | | |
|----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------------------|--|--|--|
| 153 | 136 | 130 | 133 | 146 | 168 | 197 | 231 | 269 | 308 | 342 | 369 | 389 | 403 | 413 | 423 | | | |
| 435 | 445 | 456 | 471 | 491 | 512 | 532 | 544 | 548 | 545 | 540 | 540 | 545 | 550 | 552 | 549 | | | |
| 544 | 539 | 546 | 562 | 580 | 586 | 577 | 551 | 516 | 478 | 444 | 415 | 387 | 363 | 343 | 327 | | | |
| 313 | 296 | 278 | 266 | 263 | 269 | 274 | 271 | 258 | 239 | 223 | 216 | 216 | 218 | 222 | 227 | | | |
| 232 | 237 | 240 | 239 | 232 | 217 | 196 | 173 | 153 | | | | | | | | | | |

The original TEC values given by IONEX at April15, 2015



| 32.5-180.0 | 180.0 | 5.0 | 450.0 | LAT/LON1/LON2/DLON/H | | | | | | | | | | | |
|---|-------|-----|-------|----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 153 | 136 | 130 | 133 | 146 | 168 | 197 | 231 | 269 | 308 | 342 | 369 | 389 | 403 | 413 | 423 |
| 435 | 445 | 456 | 471 | 491 | 512 | 532 | 544 | 548 | 545 | 540 | 540 | 545 | 550 | 552 | 549 |
| 544 | 539 | 546 | 562 | 580 | 586 | 577 | 551 | 516 | 478 | 141 | 415 | 387 | 363 | 343 | 327 |
| 313 | 296 | 278 | 266 | 263 | 269 | 274 | 271 | 258 | 239 | 223 | 216 | 216 | 218 | 222 | 227 |
| 232 | 237 | 240 | 239 | 232 | 217 | 196 | 173 | 153 | | | | | | | |
| The TEC values given by ZDPID program at April15, 2015 for MNSR | | | | | | | | | | | | | | | |

| 32.5-180.0 | 180.0 | 5.0 | 450.0 | LAT/LON1/LON2/DLON/H | | | | | | | | | | | |
|--|-------|-----|-------|----------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 153 | 136 | 130 | 133 | 146 | 168 | 197 | 231 | 269 | 308 | 342 | 369 | 389 | 403 | 413 | 423 |
| 435 | 445 | 456 | 471 | 491 | 512 | 532 | 544 | 548 | 545 | 540 | 540 | 545 | 550 | 552 | 549 |
| 544 | 539 | 546 | 562 | 580 | 586 | 577 | 551 | 516 | 478 | 298 | 415 | 387 | 363 | 343 | 327 |
| 313 | 296 | 278 | 266 | 263 | 269 | 274 | 271 | 258 | 239 | 223 | 216 | 216 | 218 | 222 | 227 |
| 232 | 237 | 240 | 239 | 232 | 217 | 196 | 173 | 153 | | | | | | | |
| The TEC values given by ZDPID program at April15, 2015 for Port-Said Station | | | | | | | | | | | | | | | |

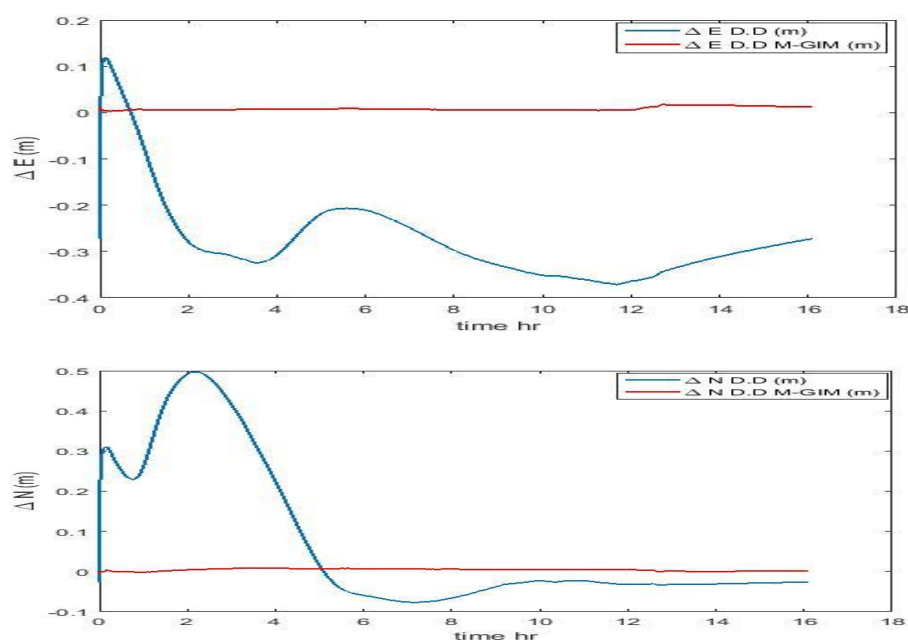
4. Results and Discussion

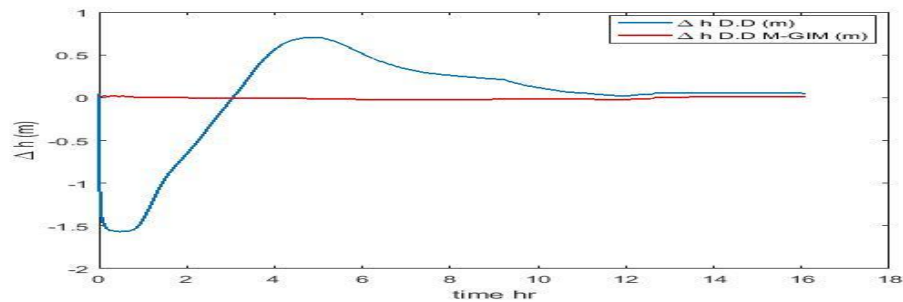
The processing of the RINEX data was conducted using Trimble Total Control 2.7. The data were processed three times: the first run was performed by using the specified baselines data with normal default processing parameters, i.e. without using GIM. The second run was carried out using modified GIM and the third run was made using static precise point positioning for all 24-hours data of all stations to be used as a threshold reference values for comparison. The CSRS-PPP was deployed to give the required static solution for the specified stations, (Rabah et al., 2016). It should be borne that the two runs of TTC solutions were obtained without fixing the ambiguities i.e. float ambiguity solution. The TTC could not fix the ambiguities for the specified baselines. The discussion is therefore based on only how the Modified IONEX files provided with the TEC values computed by the ZDIPD algorithms improve the positioning.

The differences between the CRCS-PPP solution and the two TTC positioning solution were computed and are depicted in figures 7, 8, 9 & 10. Figures 7, 8, 9 and 10 show the position differences in easting, northing and ellipsoidal height between the computed static NRCAN PPP and the kinematic epoch by epoch solution in case of normal default processing parameters (D.D) and with using modified IONEX values (D.D.M-GIM). Figure (7) demonstrates how the modified IONEX, Mod-GIM, improve the kinematic solution of the baseline Borg-Mansura with length of



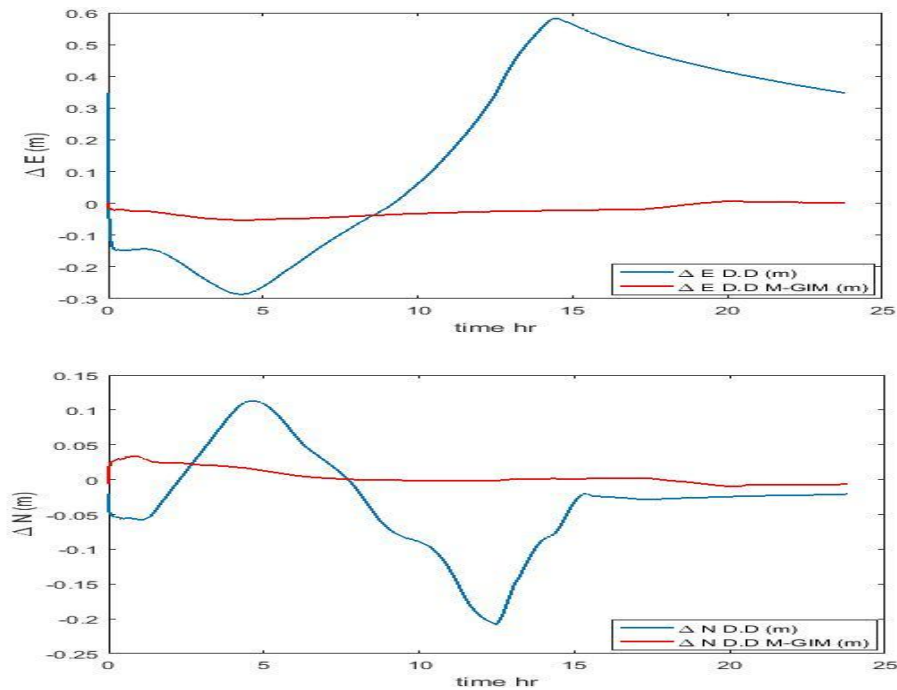
171.11 km. The differences between the two solutions were improved from (-37.11 & 11.89 cm) with RMSE 29.07cm to (0.33& 1.79 cm) and RMSE of 0.93 cm for Easting component, and for the northing component, the improvement ranged between the minimum value (-7.66 to -0.32 cm) and the maximum values was reduced from (49.71 to 0.81cm), with the RMSE improved from (19.40 cm to 0.5 cm). For the height components the differences were improved from (-156.74 & 70.55 cm) to (-2.20 & 2.00cm) with an improvement the RMSE from 54.61cm to 1.43cm. Figure (8) shows the effect of the modified Ion TEC value on improving the three components of positioning of the baseline Helwan ~ Said of length 179.51 km. The figure depicts how the Ionospheric value improve the quality and the quantity of the three positioning components. Figure (9) demonstrates how the modified Ion TEC value improved the positioning solution of the Helwan ~ Borg baselines of length 203.16 km. Finally, as it is seen in figure (10), the three components of positioning of the baseline Borg ~ Said of length 264.98 km were improved.

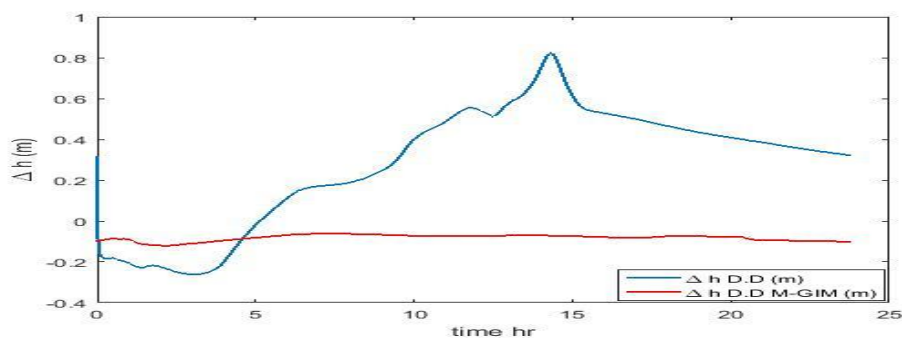




| Statistical Item | Double Diff | | | Double Diff with Mod-IONEX | | |
|------------------|-------------|------------|------------|----------------------------|------------|------------|
| | ΔE | ΔN | Δh | ΔE | ΔN | Δh |
| Min(cm) | -37.11 | -7.66 | -156.74 | 0.33 | -0.32 | -2.20 |
| Max(cm) | 11.89 | 49.71 | 70.55 | 1.79 | 0.81 | 2.00 |
| Mean(cm) | -27.42 | 7.07 | 1.03 | -0.84 | 0.42 | -0.73 |
| Rms(cm) | 29.07 | 19.40 | 54.61 | 0.93 | 0.50 | 1.43 |

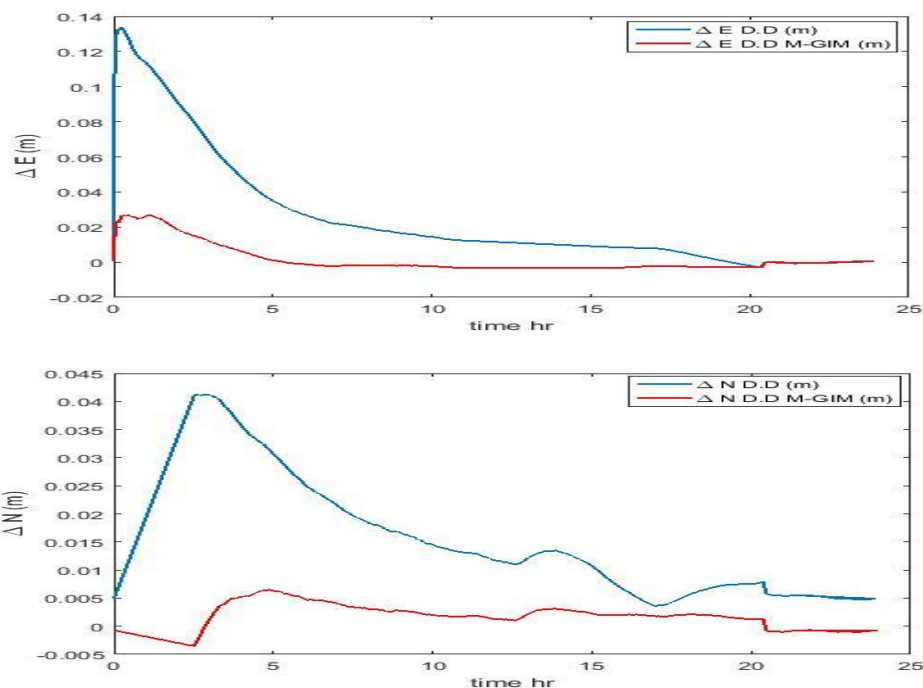
Figure (7): Positioning error with and without Mod. GIM in (East, North, Up) components between static PPP solution and relative kinematic positioning with Statistics for base line Borg~ Mnsr 171.11 km

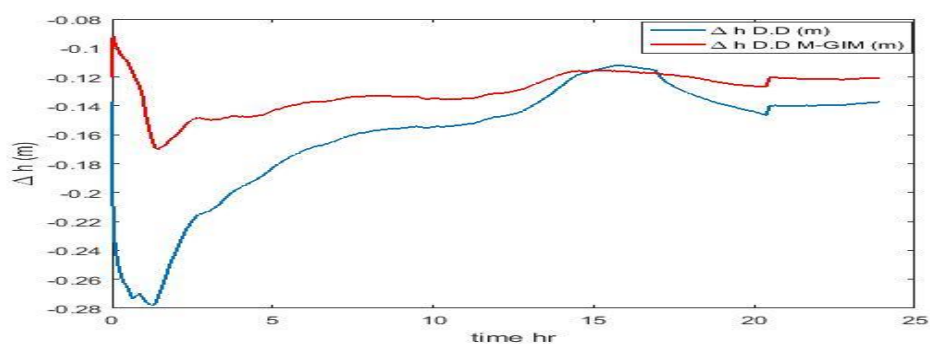




| Statistical Item | Double Diff | | | Double Diff with Mod-IONEX | | |
|------------------|-------------|------------|------------|----------------------------|------------|------------|
| | ΔE | ΔN | Δh | ΔE | ΔN | Δh |
| Min(cm) | -28.60 | -20.80 | -26.17 | -5.26 | -0.98 | -12.10 |
| Max(cm) | 58.28 | 11.31 | 82.24 | 0.81 | 3.38 | -6.25 |
| Mean(cm) | 17.00 | -3.19 | 27.78 | -2.42 | 0.38 | -8.21 |
| Rms(cm) | 34.17 | 7.76 | 40.24 | 3.01 | 1.16 | 8.35 |

Figure (8): Positioning error with and without Mod-GIM in (East, North, Up) components between static PPP solution and relative kinematic positioning with Statistics for baseline Helwan ~ Said 179.51 km.

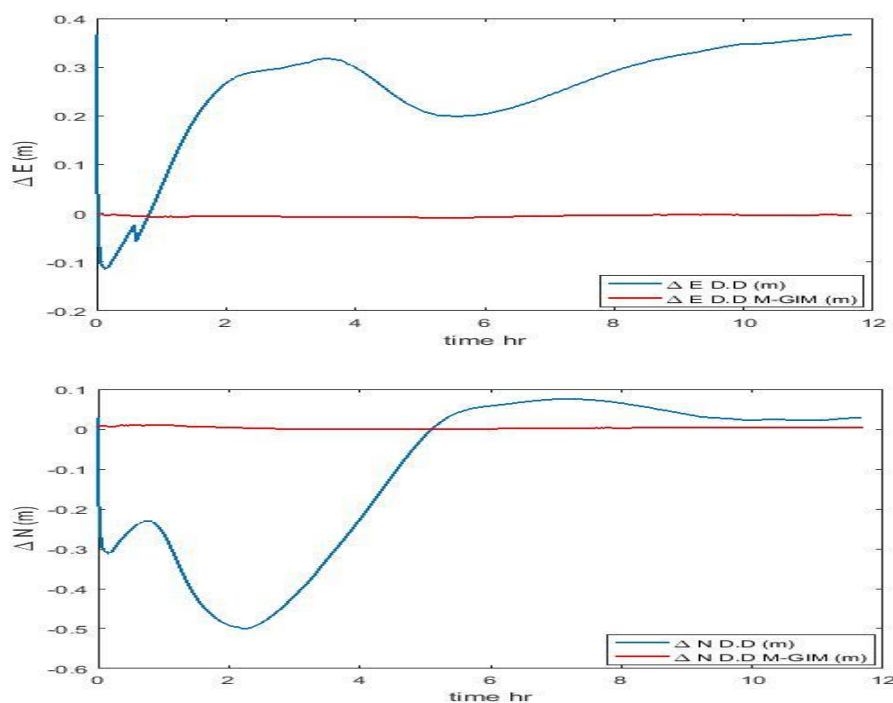


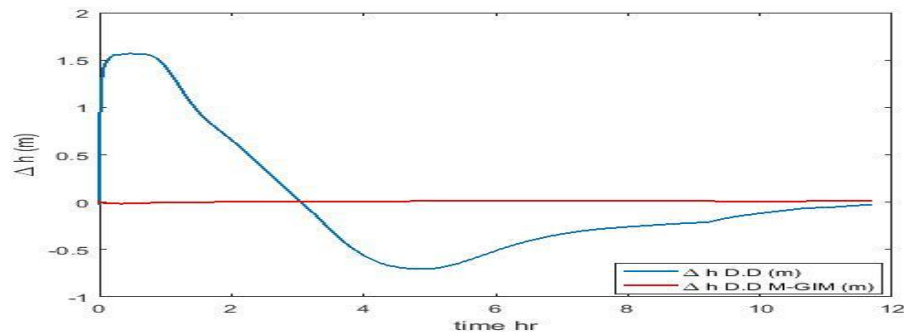


| Statistical Item | Double Diff | | | Double Diff with Mod-IONEX | | |
|------------------|-------------|------------|------------|----------------------------|------------|------------|
| | ΔE | ΔN | Δh | ΔE | ΔN | Δh |
| Min(cm) | -0.30 | 0.36 | -27.80 | -0.30 | -0.36 | -17.00 |
| Max(cm) | 13.37 | 4.13 | -11.21 | 2.68 | 0.64 | -9.21 |
| Mean(cm) | 2.90 | 1.36 | -16.05 | 0.30 | 0.18 | -13.02 |
| Rms(cm) | 4.65 | 1.70 | 16.55 | 0.92 | 0.27 | 13.08 |

Figure (9): Positioning errors with and without Mod-GIM in (East, North, Up) components between static PPP solution and relative kinematic positioning with Statistics for baseline Helwan ~ Borg 203.16 km.

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| Statistical Item | Double Diff | | | Double Diff with Mod-IONEX | | |
|------------------|-------------|------------|------------|----------------------------|------------|------------|
| | ΔE | ΔN | Δh | ΔE | ΔN | Δh |
| Min(cm) | -11.36 | -50.09 | -70.55 | -0.88 | -0.04 | -1.72 |
| Max(cm) | 36.74 | 7.54 | 156.79 | 0.20 | 1.04 | 1.86 |
| Mean(cm) | 25.07 | -11.01 | 0.43 | -0.56 | 0.32 | 0.84 |
| Rms(cm) | 27.32 | 22.77 | 64.04 | 0.59 | 0.42 | 1.13 |

Figure (10): Positioning error with and without Mod-GIM in (East, North, Up) components between static PPP solution and relative kinematic positioning with Statistics for baseline Borg ~ Said 264.98 km.

5. Conclusions

The current paper evaluates the ionospheric correction by Global Ionospheric Maps, GIM, provided in (IONEX) files produced by International GNSS Services “IGS”. The evaluation is done based on investigating the effect of given GIM ionospheric correction on kinematic relative positioning solution. The evaluation has been performed on several baselines with different lengths in Egypt. Based upon the baselines processing results, the following conclusions can be drawn:

1. Due to the lack of GPS stations over the equatorial, North Africa and Atlantic in IGS network, the produced Global Ionospheric maps (GIMs) have poor effect for mitigating ionospheric error for precise positioning.
2. Evaluation of the TEC values in IONEX map by using estimated TEC values provided by Zero-differenced phase Ionospheric Delay (ZDPID) algorithm, a fruitful result is obtained for correcting ionospheric error over kinematic solution of many baseline lengths up to 265 km.
3. Most commercial software's such Leica Geo-Office, Trimble Total Control, Trimble Business Center failed to obtain accurate results for the kinematic solution of baseline lengths over 300 km.



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