

## Interactive comment on "Beam tracking strategies for fast acquisition of solar wind velocity distribution functions with high energy and angular resolutions" by Johan De Keyser et al.

#### Johan De Keyser et al.

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#### **Reply to Reviewer Comment #1**

The authors thank the reviewer for his/her thorough revision of the manuscript and the helpful comments. Below, we respond to each of the points that was raised.

#### **General Comments**

Reviewer comment:

- Table 1 and Section 2:

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I would check to make sure that the shock jumps are correct, as I recall from the CfA Shock Database that several shocks had \$\Delta\$V > 200 km/s.
https://www.cfa.harvard.edu/shocks/wi\_data/
You should reference some recent work that provides the first long-term statistical study on solar wind parameters near 1 AU by Wilson et al. [2018] (Note the supplemental material does separate parameters by fast and slow wind).
I doubt either of these will modify the values in your table very much, but they will provide at least a reference/source for the provided values.

#### Response:

The reviewer is absolutely right in pointing out that some shocks at 1 AU involve  $\Delta V>200$  km/s. In formulating the instrument requirements, we do not require that the beam tracking algorithm should be able to capture all shocks completely, but most of them. The <200 km/s" should therefore be read as "most of the time". Checking the publication mentioned by the reviewer indeed confirms the values that we list in the table.

#### Modifications in text:

We have added a footnote in the table to point out that the values for the shock  $\Delta V$  are "most of the time" and refer there to the CfA shock list. We have added the reference suggested by the reviewer regarding typical solar wind parameters in section 2.

#### Reviewer comment:

Section 2.1: [The following are my musings, but are most likely not critical]
I see you addressed most of my concerns below in Section 3 already, but I leave it here for reference.

-- One thing of which to be careful are secondary/reflected ions near strong collisionless shocks. I assume you have thought of this and know how to handle it, but I should mention that even when the reflected to incident ion density is relatively low, it can affect the bulk flow velocity estimate determined from typical velocity moment software significantly. If the spacecraft on which the instrument of interest in this paper is to orbit Earth and not, say, L1, then bow shock reflected ions will be an issue and the fraction of reflected-to-incident is much higher (>25% in some cases) than typical interplanetary shocks. This can affect the bulk flow velocity causing it to devaiate away from the core solar wind proton beam by upwards of 30%, i.e., >100 km/s [e.g., Wilson et al., 2014a]. In the case of a sun-pointed spinner on an outbound pass, the number of reflected ions entering the detector will likely be small, so probably not an issue. However, the reflected ions at earthward propagating interplanetary shocks will always be an issue. The primary difference is that most interplanetary shocks do not reflect a significant enough fraction of the upstream ions to generate much of a foreshock, so perhaps this is not cause for concern?

#### Response:

When restricting an instrument's field of view to a cone around the solar wind direction, it is obvious that one cannot measure the reflected ions. The idea – as originally foreseen on THOR – is to have both a fast beam tracking solar wind spectrometer and an omnidirectional spectrometer (slower, offering some mass separation capability)

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operating concurrently. For THOR also the goal was to go well out into the solar wind, so as to be sure that measurements are not affected by the foreshock. Reflection from solar wind shocks indeed remains an issue.

#### Modifications in text:

In the conclusions, we have inserted a paragraph discussing the utility of combining a beam tracking instrument with an omnidirectional spectrometer.

#### Reviewer comment:

-- I know of at least one interplanetary shock that caused problems for the PESA Low detector from Wind/3DP that was seen on 2001-11-24 near 05:51 UT. The thermal energies got so large that the instrument lost the solar wind beam and did not enter tracking mode because it thought it was still following the beam. Granted, the mode was not as well designed as newer spacecraft that use NV (i.e., roughly the count rate) but it is worth considering.

#### Response:

This confirms the importance of a robust beam loss recovery strategy!

#### Reviewer comment:

-Section 3.4:

-- Be careful with the estimates of the spatial scales for discontinuities. The thickness of the shock ramp is not on ion scales, but on electron scales [e.g., Hobara et al., 2010; Mazelle et al., 2010]. What is not shown in the Spektr-R data is what was assumed for years to be the actual shock ramp but was undersampled [e.g., see Wilson et al., 2012, 2017]. In general, I think your estimates are fine, but the statement that ion properties cannot change faster than ion scales is factually incorrect. Further, it is not the case that the fluctuations discussed in the above references have no effect on the ions, as shown by Goncharov et al. [2014].

#### Response:

Agreed. The ion gyroradius is a characteristic of the spatial scale of variation of the ion VDFs, but the scale can be smaller if the magnetic field changes more rapidly and/or if there are strong localized electric fields – and there the electron scales can come into play.

#### Modifications in text:

We have reformulated this paragraph, and refer to Mazelle et al. (2010) and Krasnoselskikh et al. (2013) who discuss spatial scales in shocks.

#### Reviewer comment:

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- Section 4.1
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-- I am confused. If you have a sun-pointed spinning spacecraft and you align the central elevation angle bin with roughly the Earth-sun line, why does the solar wind beam vary with spin in the elevation angle? Or am I misunderstanding Figure 1 and the discussion in this section? Is the spacecraft spin axis not aligned with the Earth-sun line?

#### Response:

The goal here is to illustrate what happens if the solar wind arrival direction does not coincide with the spacecraft spin axis. That is going to happen very often. There is the solar wind aberration angle that changes continuously within a range of a few degrees. But it is also very unlikely that the spacecraft spin axis not aligned with the Earth-sun

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line. Indeed, suppose the alignment is perfect at a given instant, it will be  $360^{\circ}/365.25 = 1^{\circ}$  off one day later because the spinning spacecraft axis keeps a constant direction in an inertial frame. Spacecraft operators would not want to do manoeuvres to reorient the axis on a daily basis (and the scientists wouldn't like that either).

### Modifications in text:

We do think the explanation in 4.1 is clear enough.

#### Reviewer comment:

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-- Page 7, Lines 27-30: I do not follow the sentence starting with "The difference between..." Is this a comment on the results shown in Figure 1 or a general comment about the solar wind?
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#### Response:

That is a comment regarding the results. We simply want to point out that the measured arrival direction matches quite closely the true values with which we have set up the simulation.

# *Modifications in text:* We have adapted the phrase for clarity.

#### Reviewer comment:

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-- Page 8, Lines 4-5: Can you be a little more quantitative
with the statement "...distributions are somewhat distorted..."?
Distorted in what way? Would one interpret the VDFs as having a
higher temperature than reality, for instance? If so, by how much?
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#### Response:

The errors in arrival direction are quantified in Figure 2. The VDF distortion is illustrated in Figure 3. "Rotational smearing" of the VDFs will not affect the mean energy that is

measured, but it affects the mean arrival direction angles and it leads to a temperature anisotropy. Such high spacecraft spin rates are undesirable anyhow and one should stay away of that regime.

#### Modifications in text:

We inserted a phrase to describe the nature of the distortion more clearly (but still rely on Figure 3 to illustrate it).

#### Reviewer comment:

#### - Section 4.3

-- Having had several long conversations with Drs. Safrankova and Nemecek (a few years ago now) about the capabilities and limitations of the BMSW instrument, I am curious how you managed to get the data into GSE coordinates. It was my understanding that there is no way to know the actual spacecraft orientation and attitude necessary to rotate the data out of spacecraft coordinates into a physically meaningful basis. Has this issue been recently resolved?

#### Response:

The instrument is mounted on the solar panels which can rotate. The exact solar panel rotation angle is not always known, which renders it impossible to derive the exact instrument look direction. However, for a considerable fraction of the time, including the events considered here, the solar panel rotation angle is fortunately available (though at a limited time resolution) and so the data can effectively be rotated into the GSE frame. We are particularly thankful to the referee for asking this question: digging deeper into this matter, we found out that we had actually NOT used the data in the GSE frame, but in the instrument frame, which, for the shock event, had its x-axis pointing about  $11^{\circ}$  away from the sun.

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#### Modifications in text:

We have rerun the simulations for examples 7-8-9 using the data in the GSE frame and we have updated the figures. Note that, while we had originally observed that the solar wind seemed to go out of the CSW field-of-view, this now no longer is the case – this was simply due to the off-pointing x-axis. In retrospect, this should have triggered us to be suspicious of the reference frame of the original data. We have made the corresponding modifications in the text where we discuss these simulations. The paragraph in the conclusions that commented on the CSW field-of-view was also adapted.

#### Reviewer comment:

-- The shock on 2015-06-22 arrived at L1 at ~18:08:24 UT (e.g., I looked at Wind data on CDAWeb). Regardless, the bulk flow velocity along X-GSE jumps to nearly -800 km/s in the downstream and the ion temperature exceeds 100 eV (i.e., ~1.2 MK), so the temperatures may not be too inaccurate from BMSW. The CfA shock database shows a density compression ratio of ~3.4 but I think the temperature changes by a factor >4-5. [These are just comments, not really actionable items.]

-- Page 9, Lines 50-51: Are the temperature and temperature anisotropy significantly affected as well, or just the density moment?

#### Response:

Thanks for checking this shock with the Wind data. It can indeed be interesting to try to compare some of the BMSW data with shock measurements elsewhere in geospace. As stated in the text, the temperature measurement is affected too. BMSW does not provide temperature anisotropy.

Reviewer comment:

#### - Hot and/or Tenuous VDFs

-- One of the biggest issues that I did not see addressed in the manuscript occurs during intervals when the density is low [i.e., below ~1 cm^(-3)] or the temperature is high (i.e., Ti > ~100-200 eV, depending on the instrument). If we assume a bi-Maxwellian or even an isotropic Maxwellian, the peak phase space density goes as  $N*T^{(-3/2)}$ . The one-count level during the same interval does not drop/change relative to an adjacent, earlier interval. Thus, the signal-to-noise ratio can drop preciptously during these periods. I realize this is an issue faced by all particle instruments, but it is worth discussing to ensure you do not lose the critical parts of the distribution downstream of strong shocks with high temperatures but relatively low density (e.g., for really low upstream density).

#### Response:

The referee is absolutely right in stressing the importance of making sure that there are no problems with the signal-to-noise ratio. We want to point out 3 elements in this respect:

 As mentioned in the introduction, any plasma spectrometer faces a trade-off between (a) angular and energy resolution, (b) time resolution, (c) signal-to-noise ratio. Obviously this trade-off is linked to hardware limitations (e.g. the instrument's geometrical factor is limited by the volume and mass budget, there are constraints due to the telemetry budget, etc...). It is precisely here that beam tracking is useful: by making measurements only where it matters, the best tradeoff remains possible. For instance, for given time, angular and energy resolutions, beam tracking allows to maximize the data collection time per measurement bin

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so that even for low count rates a significant number of counts can be collected, thereby improving the signal-to-noise ratio. So implementing beam tracking in general helps to avoid low counts.

- The important question here is whether the beam tracking strategy would not get confused in low density / high temperature environments. With the simple beam loss detection strategy used here, low densities would trigger the "beam loss" condition. But that would not be dramatic: the instrument simply returns to a measurement strategy that samples the full phase space accessible by the instrument. Although one would lose time resolution, providing VDFs over the full phase space is one of the best things one can do in such a situation (especially for the high temperature case). A posteriori, one can bin the measurements in energy, azimuth, elevation and/or time to improve the signal-to-noise ratio even further so that these measurements are scientifically useful.
- Beam tracking driven by a Faraday cup instrument would suffer less from problems in such situations, since a Faraday cup inherently provides a better signalto-noise as it integrates the particle flux over its entire field of view.

#### Modifications in text:

We have inserted a paragraph in section 3.3 (Beam loss detection and recovery) discussing this matter.

#### **Minor Concerns**

#### Reviewer comment:

-- Page 1, Lines 35-50: You could also mention waves and instabilities [e.g., Malaspina et al., 2013], as electromagnetic fluctuations are not solely limited to turbulence. It is also important to measure the full 3D

VDFs for analysis of instabilities.

#### Modifications in text:

Sure. We have added a sentence + a few references.

*Reviewer comment:* – Page 2, Lines 2-18: The Wind spacecraft's 3DP instrument suite is also relevant here [e.g., Lin et al., 1995].

#### Modifications in text:

We have added a sentence about 3DP (mentioning also its higher angular resolution near the ecliptic plane) as well as the reference.

#### Reviewer comment:

-- Page 2, Line 47: I know voxel is a term analogous to a velocity-space pixel, but could you provide a definition for the reader that may not know this.

#### *Modifications in text:* Provided a definition upon first occurrence

#### Reviewer comment:

-- Page 7, Lines 10-12: I am not sure I understand the sentence starting with "It starts measuring..." You state the instrument starts sampling at 600 ms and the duration required to obtain one full VDF is another 600 ms. Is that correct?

*Response:* Yes, absolutely correct.

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#### Typos, Grammar, etc.

Reviewer comment:

[The following are suggestions, not requirements (e.g., I do not recall rules for British vs. American grammar for when to use commas after things like "e.q." or "i.e.")] Page 4, Line 25: "12, i.e. an order" --> "12, i.e., an order" Page 5, Line 56: "i.e. one uses" --> "i.e., one uses" Page 5, Lines 77-79: "In order to eliminate values that are completely off, a voting" -->"In order to eliminate outliers, a voting" Page 5, Line 87: Try rephrasing the following "Note that such a more robust procedure requires" as it is awkwardly phrased and not clear what is meant. Page 6, Line 38: "robust (i.e. when" --> "robust (i.e., when" Page 6, Line 40: "...cient (i.e. when" --> "...cient (i.e., when" Page 6, Line 98: "direction (i.e. with" --> "direction (i.e., with" Page 8, Lines 62-63: "The measurement points" --> "The measurements" Page 9, Line 19: "neither dramatic in magnitude nor very" --> "neither dramatic in magnitude or very" Page 11, Line 5: "instrument (i.e. of" --> "instrument (i.e., of"

#### *Modifications in text:* Thanks, all have been dealt with.

manks, all have been dealt with

#### Reviewer comment:

Page 14, Line 5: "manoeuvres" --> "maneuvers"

## *Response:* We stick with British English.

#### References

-- Goncharov, O., et al., "Upstream and downstream wave packets associated with low-Mach number interplanetary shocks," Geophys. Res. Lett. 41, pp. 8100---8106, doi:10.1002/2014GL062149, 2014. -- Hobara, Y., et al., "Statistical study of the quasiperpendicular shock ramp widths," J. Geophys. Res. Vol. 115, pp. A11106, doi:10.1029/2010JA015659, 2010. -- Lin, R.P., et al., "A Three-Dimensional Plasma and Energetic Particle Investigation for the Wind Spacecraft," Space Sci. Rev. Vol. 71(1), pp. 125--153, doi:10.1007/BF00751328, 1995. -- Malaspina, D.M., et al., "Electrostatic Solitary Waves in the Solar Wind: Evidence for Instability at Solar Wind Current Sheets," J. Geophys. Res. Vol. 118, pp. 591âĂŤ599, doi:10.1002/jgra.50102, 2013. -- Mazelle, C., et al., "Self-Reformation of the Quasi-Perpendicular Shock: CLUSTER Observations, " Proc. 12th Int. Solar Wind Conf., AIP Conf. Proc. 1216, pp. 471--474, doi:10.1063/1.3395905, 2010. -- Wilson III, L.B., et al., "Observations of electromagnetic whistler precursors at supercritical interplanetary shocks," Geophys. Res. Lett. Vol. 39, L08109, doi:10.1029/2012GL051581, 2012. -- Wilson III, L.B., et al., "Quantified energy dissipation rates in the terrestrial bow shock: 1. Analysis techniques

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and methodology," J. Geophys. Res. Vol. 119, pp. 6455--6474, doi:10.1002/2014JA019929, 2014a. -- Wilson III, L.B., et al., "Revisiting the structure of low-Mach number, low-beta, quasi-perpendicular shocks," J. Geophys. Res. Vol. 122, pp. 9115--9133, doi:10.1002/2017JA024352, 2017. -- Wilson III, L.B., et al., "The Statistical Properties of Solar Wind Temperature Parameters Near 1 au," Astrophys. J. Suppl. Vol. 236(2), pp. 41, doi:10.3847/1538-4365/aab71c, 2018.



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#### **Reply to Reviewer Comment #2**

The authors thank the reviewer for his/her thorough revision of the manuscript and the helpful comments. Below, we respond to each of the points that was raised.

#### **General Comments**

Reviewer comment:

The presented manuscript presents and discusses a novel

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approach to employ electrostatic spacecraft analyzers fitted with angular deflectors. By evaluating beam parameters of the surrounding plasma, only energyand directional bins relevant to resolving said beam need to be sampled, resulting in much faster signal acquisition and as a result, higher time resolution.

The presented method represents an instance of a sparse sampling approach, in which the sample points from a high-dimensional parameters space are deliberately constrained to certain subsets of that space in order to obtain a maximum amount of information with minimal sampling requirements. Similar techniques have been employed with great success in Biophysics (Such as compressed sensing techniques in neurosciences [1]), Astronomy (in aperture synthesis for telescopes [2]). Likewise in the same field as this manuscript, kinetic simulation approaches in space physics employ similar techniques to reduce the computational load of highdimensional simulation spaces [3,4].

References to similar approaches from those fields, as well as overview papers of compressed sensing methods should be added, since a large body of general theoretical background work from other fields can be applied for this approach.

Specifically, the presented manuscript discusses a method to sparsely sample space plasma velocity

distributions, with the intention of tracking a "beam" and sampling it with a minimum number of required samples, to obtain an extraordinarily high temporal resolution.

#### Response:

Indeed, beam tracking tries to represent a system with a maximum amount of information for a minimum sampling effort. That there is a general theoretical framework regarding "sparse sampling" is undisputable. However, we feel somewhat reluctant to expand the manuscript with a discussion of the "sparse sampling" or "compressed sensing" context for two kinds of reasons.

First: How relevant is "sparse sampling" or "compressed sensing" in this context?

• The "compressed sensing problem" deals with reconstructing a sparse vector from a reduced number of data with sparsity as a priori knowledge. The idea then is that measuring the limited data is sufficient to reconstruct the full data if one knows the sparsity properties. The practical relevance of this is very much dependent on the specific assumptions. "Beam tracking" is a very specific form of sampling, in which knowledge about smoothness and compactness of the VDFs in velocity space, and physical knowledge about the time scales involved, are all fundamental. In other words: the peculiarities of the situation at hand are responsible for the fact that one cannot learn very much from the generic theory. To put it simply: We measure data in a compact subregion of phase space (the reduced data), and from that we derive the full data by simply assuming that the VDF is zero outside that subregion (finding the full data from the known sparsity pattern). This sort of application is so trivial that we do not need the general theory. Of course, more refined approaches could be possible in which one might sample a few isolated points in phase space to derive the full VDF from that, but this would be strongly dependent on specific assumptions (for instance, you could

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do this efficiently if you assume that the distribution is a bi-maxwellian). However, the scientists usually do not want to make those assumptions. Alternatively, one might train a subsampling algorithm on a set of realistic data ... but we do not have such training data – we have at present no high time cadence VDFs.

- The standard "compressed sensing" theory does not take into account the notion that there might be variable costs associated with collecting the reduced data. There is a cost (a time delay) associated with switching the spectrometer to a different energy (due to the need to set high voltages and the accompanying settling times). It makes little sense to measure at a specific elevation angle, since it is much more time-efficient to sweep the voltage between the deflector plates to acquire a contiguous set of measurements over all elevations at once. All these practical constraints limit the amount of sparsity in the problem, so that there is little to gain from the general approach.
- Compressed sensing has a lot in common with data compression, in particular with lossy compression. That is something that scientists prefer to avoid. To really understand the measurements, and to be able to reprocess data, they prefer not to work with an "indirect" representation of the sampled velocity space (the reduced data set); they simply want to know the values as measured in all the individual voxels, not any reconstructed values. Indeed, it would be very awkward (though not impossible) to update an instrument calibration and reprocess the raw data if only an indirect representation is given.
- An additional problem with an "indirect representation" is that any further statistical analysis of the data will be hampered by the strong and specific crosscorrelations between the errors on the measurements in different voxels.
- For beam tracking and moment calculation, one must be able to interpret the measured data on-board in a straightforward manner and fast. It is not at all clear whether the typical optimization techniques used in compressed sensing and

the required response times are within the capabilities of present-day on-board processors.

Second: How relevant is it to mention "sparse sampling" for the reader of the paper?

- Our introduction briefly reviews a number of plasma spectrometers, showing the progress of technology and actually focusing on the way in which the velocity space sampling problem has been approached. That sketches the context for the discussion of beam tracking sufficiently well to allow the reader to follow the text. We are therefore not convinced of the necessity of inserting an overview of sparse sampling techniques in the introduction.
- We want to point out that every measuring instrument is doing one form or another of sparse sampling, yet descriptions of instruments typically do not mention sparse sampling theory (none of the reference papers for the plasma spectrometers that are reviewed in the introduction does). Admittedly, it is not because nobody does it, that it could not be useful.
- We are already a bit concerned about the manuscript length and do not want to expand it unnecessarily.

#### Modifications in text:

Given all the above, we have inserted a paragraph that mentions the possibility to interpret beam tracking in the context of "sparse sampling" or "compressed sensing", without entering into a deeper discussion that would necessitate to mention some of the points listed above. We have chosen to do so in the discussion section, rather than in the introduction. This allows us to present sparse sampling methods as a possible future avenue in the quest for even faster solar wind characterization. We have added a few general references, and one targeted toward the space plasma physics audience.

Reviewer comment:

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The model assumptions going into the example analysis performed in this manuscript are a) that the "interesting" part of the particle distribution is quite compact in shape, more precisely, in this analysis it is assumed to be maxwellian b) that it's overall shape stays the same, and only it's parameters change. These assumptions preclude the possibility of multiple mixed plasma distributions, such as a core and beam setup in a foreshock, rings or loss cones in a fermi-type acceleration region or any other non thermally-relaxed particle distribution.

I assume that the authors only focus on the solar wind distributions' core is motivated by their specific research interests. However, the study of kinetic physics of the solar wind, including the effects of turbulence, shocks and magnetic reconnection depends strongly on the ability to study and understand nonthermal distribution functions, that is, precisely those distribution functions that do not fulfill the assumptions going into the manuscript at hand.

#### Response:

There seems to be a serious misunderstanding here. We make no assumption regarding the shape of the velocity distribution function other than that it is compact, i.e., that it occupies only part of the phase space accessible by the instrument. We use Maxwellians only to test the beam tracking algorithm, since we do not possess any VDF measurements at the high cadence considered here. The shape of the distribution is allowed to change, it can be anisotropic, it can consist of a core and halo, it can be a mixture of different populations, the particle distribution does not have to be thermally relaxed ... as long as the compactness condition is satisfied. The degree to which this must be the case depends on the choice of the phase space energy/azimuth/elevation window sizes. Obviously, this approach cannot deal with non-compact distributions. It precludes, for instance, the detection of backstreaming solar wind particles reflected from an interplanetary shock: an instrument staring at the sun cannot detect particles coming from behind.

#### Modifications in text:

Also in view of a comment by the other referee, we have inserted a paragraph in the conclusions that addresses the issue of populations reflected from shocks.

#### Reviewer comment:

While a much more thorough analysis and quantification of the detector behavior for realistic distribution functions will be required before the presented method can be employed in an actual instrument, it is probably not within the scope of this paper to perform them -the central subject and conclusion being the presentation and motivation of a sparse sampling scheme in the first place. Still, some more reflection on the limitations of the presented analysis, and avenues to further refine the analysis should be included.

In conclusion, this manuscript presents a thoroughly novel idea that merits publication and discussion in the wider scientific community, but suffers from being too narrow in it's goals and scope. After some major revisions, in which the presented method is evaluated

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with a focus on more general kinetic-physics processes, I consider it suitable for publication.

#### Response:

We're a bit surprised that the reviewer asks us to evaluate the method with a focus on general kinetic physics requirements, as we believe that the present manuscript does exactly that. Indeed, studies of turbulence, waves, or instabilities require only two things of a plasma spectrometer: (a) obtain VDFs with high energy and angular resolution, and (b) with high time resolution. That the first goal can be achieved with the THOR-CSW design parameters, has been demonstrated by Valentini et al. (2016) as cited in the manuscript. The present study of beam tracking demonstrates that the first goal can be achieved while at the same time satisfying the second goal. That demonstration consists of

- Showing that with realistic sizes of the beam tracking window and the prescribed angular and energy resolutions, a high time resolution can be achieved.
- Showing that and this is what we perceived as being the major concern the beam tracking technique is able to deal with dramatic time evolution in the solar wind, as exemplified by shocks. There is no reason to worry about rapid, but less dramatic, changes at or near the centre of the solar wind beam: they will be captured as long as the beam tracking window is large enough.

The description of how beam tracking can be implemented, as well as the examples, corroborate our claim that beam tracking is indeed capable of leading to solar wind VDF measurements that enable (ion) kinetics-physics studies.

### Specific Comments

Reviewer comment:

The prediction method presented in section 3.2 and it's discussion of polynomial extrapolation overshoots is very similar in nature to the problem of flux limiters in finite volume simulation methods, such as MHD simulation. There, too, the extrapolation of a reconstruction polynomial is clamped to remain within physically realistic boundaries. This similarity could be discussed and referenced (such as [5]).

#### Response:

There is indeed a certain similarity with flux limiters used in computational fluid dynamics, but the setup is different: in the CFD case, one knows the gradients at both sides of an interface, and the ratio between those two gradients is used as the argument of the flux limiter to bound the extrapolations from either side. In the case of beam tracking, one only knows the gradient from the past; nothing is known about the future. Actually, there are numerous other situations where an extrapolation (which is always risky) can be bounded by using additional heuristic knowledge. Stock market prediction is actually much more similar to the beam tracking problem that we are dealing with. However, we think that making that comparison in the manuscript would lead us too far astray.

#### Reviewer comment:

The same section claims that "All in all, one can expect such techniques to work reasonably well only if the energy does not change rapidly", and I agree with that statement. However, especially in shocks, discontinuities and reconnection regions, where this assumption does not hold true, is where the most interesting kinetic plasma physics effects occur.

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#### Response:

This sentence refers specifically to the use of higher order polynomial interpolation. The point that we make here is that linear interpolation is actually better in view of shocks or discontinuities, as explained in the preceding sentence.

#### Modifications in text:

We have rephrased the sentence to avoid any misunderstanding.

#### Reviewer comment:

Note that the sudden changes of distribution function in these events are not simply a parameter change of a maxwellian: the shape of the distribution function departs \*significantly\* from a maxwellian whenever kinetic physics comes into play. If the spacecraft changes it's magnetic connection to a shock, beam distributions of highly nonthermal shape can suddenly "appear" outside of the thermal velocity radius of the previous maxwellian. In reconnection regions, spitzer orbits and crescent-shaped velocity distributions additionally appear on top of any thermal background that might still be present. Additionally, nonisotropic superthermal tails can deform the solar wind distribution away from a maxwell-boltzmann shape.

#### Response:

We reiterate that we make no assumption regarding the shape of the velocity distribution function that has to be measured, although our tests are limited to Maxwellian distributions. We understand very well the risks of monitoring only a limited part of phase space – indeed, one can miss certain features. This is why a beam tracking plasma spectrometer is best used in combination with an omnidirectional spectrometer, where the former gives you very high time resolution for the core of the distribution, and the latter provides the full context (but probably at a slower pace).

#### Modifications in text:

A paragraph inserted in the conclusions addresses this complementarity of both types of spectrometer.

#### Reviewer comment:

The discussion in section 4.4, comparing internal and external beam tracking, is thus incomplete, as the asumption of a continuous change of maxwell distribution parameters won't represent reality in many interesting kinetic physics scenarios.

#### Response:

Maxwellian distributions are used here only to construct a test example. The emphasis of the test in section 4.4 is on achieving the necessary time resolution and being able to follow the rapid velocity jumps (jumps in energy and/or beam direction). The reviewer is of course correct in that the changing nature of the distributions themselves could play a role as well; in that sense the test is indeed incomplete. However, nobody has ever measured distributions that rapidly, so we had to construct the example artificially. An alternative could have been to use the output of a full Vlasov simulation code, but we do not have access to such simulations over a sufficiently long time period and featuring solar wind shocks. It is our opinion that "the proof of the pudding is in the eating", i.e., a full evaluation of beam tracking is only possible by building an instrument and trying it out in space.

#### Modifications in text:

We have inserted a short discussion concerning the incompleteness of the test as the

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last paragraph in section 4.3 (this issue is applicable to all the tests with the BMSW data, and goes beyond the internal/external beam tracking differences).

## Reviewer comment:

As for the beam loss criterion itself (sections 3.3 and 3.4), it is based on the assumption that the "beam" encompasses the entire interesting part of the distribution function at time of tracking, and that the only noteworthy change at a plasma discontinuity would be a sudden loss of the beam at one spot, with reappearance at another. This is a rough oversimplification of the wide variety of foreshock distribution functions (compare [6]): in many cases, additional beam distributions will occur far outside the thermal velocity extents of the solar wind beam, thus remaining untracked by the restricted sampling process presented here. "Beam Loss" as defined in this paper is neither an appropriate, nor a sufficient criterion for re-scanning of the complete velocity space.

#### Response:

No, the beam tracking spectrometer can follow all sorts of changes in the shape of the distribution functions across a discontinuity, as long as these occur not too far away from the centre of the beam. We agree that this condition is not valid in the foreshock. As mentioned before, this is why a beam tracking plasma spectrometer is best used in combination with an omnidirectional spectrometer.

Modifications in text: This is now addressed in the conclusions section. Reviewer comment: The presented tests inadequately asses the response of the method to these kind of scenarios. While it is good and correct to assess the ability of this method to reacquire the beam after a beam loss scenario with realistic dynamic timescales, this is, by far, not the only relevant measurement quantity to optimize for. I would suggest expanding section 4 with a discussion of the applicability of the presented method for the study of nonthermal kinetic effects in the distribution function. This can be rather open-ended, to initiate constructive discussion about the proposed method: estimates of dynamic timescales, angular extents and energy ranges would already allow the method to be scrutinized by experts specializing on specific phenomena.

#### Response:

What the reviewer proposes here goes far beyond the demonstration of beam tracking as a viable method to operate a plasma spectrometer so as to satisfy the generic requirements for doing kinetic-scale physics. A detailed examination of what can be done by a specific spectrometer with given energy/azimuth/angular and time resolutions for a particular set of non-thermal kinetic effects (as simulated by a Vlasov code) could indeed be the subject of a follow-up paper.

#### **Technical Corrections**

Reviewer comment:

Simulated measurement plots (figures 1, 3, 5, 7, 8 and 9) are missing an axis label on their (presumably) time axis.

Modifications in text:

C13

We added the axis label on all those plots.

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## Interactive comment on "Beam tracking strategies for fast acquisition of solar wind velocity distribution functions with high energy and angular resolutions" by Johan De Keyser et al.

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In the supplement, the authors provide the revised manuscript, marked up to highlight the modifications that were made.

Please also note the supplement to this comment: https://www.ann-geophys-discuss.net/angeo-2018-59/angeo-2018-59-AC3supplement.pdf

Interactive comment on Ann. Geophys. Discuss., https://doi.org/10.5194/angeo-2018-59, 2018.

C1

# Beam tracking strategies for fast acquisition of solar wind velocity distribution functions with high energy and angular resolutions

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**Abstract.** Space plasma spectrometers have often relied on spacecraft spin to collect three-dimensional particle velocity distributions, which simplifies the instrument design and reduces its resource budgets, but limits the velocity distribution acquisition rate. This limitation can in part be overcome by a the use of electrostatic deflectors at the entrance of the analyser. By mounting such a spectrometer on a sun-pointing spacecraft, solar wind ion distributions can be acquired at a much higher rate because

- 5 the solar wind ion population, which is a cold beam that fills only part of the sky around its mean arrival direction, always remains in view. The present paper demonstrates how the operation of such an instrument can be optimized optimized through the use of beam tracking strategies. The underlying idea is that it is much more efficient to cover only that part of the energy spectrum and those arrival directions where the solar wind beam is expected to be. The advantages of beam tracking are a faster velocity distribution acquisition for a given angular and energy resolution, or higher angular and energy resolution for a given
- 10 acquisition rate. It is demonstrated by simulation that such beam tracking strategies can be very effective while limiting the risk of losing the beam. They can be implemented fairly easily with present-day on-board processing resources.

Keywords. Interplanetary physics (instruments and techniques, solar wind plasma)

Copyright statement.

#### 1 Introduction

15 The plasma in the outer layers of the solar atmosphere is so hot that even the sun's gravity cannot restrain it. The sun therefore produces a persistent stream of plasma that flows almost radially away in all directions. This "solar wind" consists of electrons and ions (protons with a limited admixture of alpha particles and trace amounts of highly ionised heavier elements) and constitutes an overall electrically neutral plasma. The solar wind can be regarded as a turbulent medium that is driven by free energy from the differential motion of plasma streams that cascades via Alfvén waves down to kinetic scales where it is dissipated (e.g. Coleman, 1968; Tu and Marsch, 1995; Bruno and Carbone, 2005)(e.g., Coleman, 1968; Tu and Marsch, 1995; Bruno and Carbone, 2 . Studies of solar wind turbulence at kinetic scales require the acquisition of full three-dimensional velocity distribution functions (VDFs) with high energy resolution and high angular resolution at a rapid cadence to be able to observe vari-

- 5 ous signatures of the underlying processes in the VDFs (e.g. Marsch, 2006, 2012; Kiyani et al., 2015; Valentini et al., 2016) (e.g., Marsch, 2006, 2012; Kiyani et al., 2015; Valentini et al., 2016), while maintaining a sufficient signal-to-noise ratio. Also the study of plasma waves and instabilities requires detailed and fast solar wind VDF measurements (e.g., Marsch et al., 1982, 2006; Mattei Achieving all these objectives at the same time is a daunting task that places stringent performance requirements on plasma spectrometer hardware.
- 10 On early solar wind missions such as Helios 1 and 2 (Porsche, 1981), where the satellite spin axis was perpendicular to the ecliptic, the plasma instruments actively scanned over energy by rapidly stepping the analyser potential, simultaneously measuring over a range of angles in the plane containing the spin axis, while scanning over angles in the plane perpendicular to the spin axis with spacecraft rotation (Rosenbauer et al., 1977, 1981). The spacecraft spin rate (60 s in this case) is the maximum solar wind VDF time resolution that can be achieved with such a setup, unless multiple instrument heads are installed (as
- 15 has been done, for instance, for the Fast Plasma Investigation instruments on NASA's Magnetospheric MultiScale spacecraft (Pollock et al., 2016)). A similar situation occurs on the Cluster satellites (Escoubet et al., 2001). Their 4s spin period thus leads to a correspondingly better time resolution for solar wind measurements with the CIS-HIA instrument (Rème et al., 2001). The PESA detectors in the 3DP instrument on Wind (Lin et al., 1995) utilise a variable angular resolution (higher resolution near the ecliptic plane) to optimise solar wind beam measurements, but remain limited by the 3s spin period. To do even better, one
- 20 must ensure that the solar wind always remains in the field of view of the detector. This can be achieved with a 3-axis stabilized stabilised platform (e.g., Solar Orbiter (Müller et al., 2013)) or with a spinning spacecraft that has its spin axis pointing toward the Sun (e.g., as was proposed for THOR (Vaivads et al., 2016)). An instrument that always looks at the Sun, however, must create a VDF by sampling different energies and directions simultaneously by using multiple detectors or by actively scanning over energies and directions, or a combination of both. For example, the BIFRAM spectrometer on Prognoz 10 used a hybrid
- 25 approach, with multiple analysers simultaneously sampling along the Sun–Earth line and scanning over energy in a time-shifted way to obtain a 63 ms time resolution, and at the same time using several detectors pointing from 7° to 24° away from the solar direction along different azimuth angles; while not covering the full sky, combining these data leads to representative energy spectra with a time resolution of 640 ms (Vaisberg et al., 1986; Zastenker et al., 1989), a rate much faster than the spacecraft spin (118s). Another approach is to have multiple detectors over only one angular coordinate (azimuth) but to scan actively
- 30 over energy and the other angle (elevation). This can be implemented by placing a deflector system in front of the spectrometer entrance, as has been done for SWA-PAS on Solar Orbiter (Marsden and Müller, 2011) and as has been envisaged for the THOR-CSW ion spectrometer (Cara et al., 2017). Such instruments need a high geometric factor to ensure an appropriate signal-to-noise ratio even with short exposure times. Short exposures are a necessity if the full VDF must be obtained rapidly, especially if the number of energy and elevation bins is high.

#### Table 1. Solar wind parameters at 1 au and instrument requirements

Parameter	slow wind	fast wind
Speed $[\text{km} \cdot \text{s}^{-1}]$	350	800
ICME speed $[\text{km} \cdot \text{s}^{-1}]$	< 2000	< 2000
Shock speed jumps $[\text{km} \cdot \text{s}^{-1}]$	$< 200 \leq 200^{\mathrm{a}}$	$< 200 \leq 200^{\mathrm{a}}$
Proton thermal speed $[\mathrm{km}\cdot\mathrm{s}^{-1}]$	20-40	40-80
Tangential speed jumps $[\text{km} \cdot \text{s}^{-1}]$	< 80	< 80
Energy range [eV]	640	3330
ICME maximum energy [eV]	< 20000	< 20000
Shock energy jumps [eV]	900	1900
Proton thermal energy [eV]	2-8	8–33
<i>Required energy range</i> [eV]	600 to 20000	
Minimum energy window $\stackrel{{\tt a\_b}}{\sim}$	5%	
Recommended energy window $\stackrel{a \ b}{\sim}$	20–30 %	
Solar wind aberration $\frac{b}{c}$ [°]	3–7	1–3
Range of direction [°]	-13 to $+13$	-6 to $+6$
Thermal beam width $[^{\circ}]$	-7 to $+7$	-6 to $+6$
<i>Required angular range</i> [°]	-24 to $+24$	
Minimum angular window <sup>a_b</sup> [°]	24	

<sup>a</sup> Most of the time; occasionally, shock speed jumps can be higher, see *https://www.cfa.harvard.edu/shocks/wi\_data/*.

 $^{\rm b}$  Windows are computed between  $\pm 2$  standard deviations.

<sup>c</sup> The solar wind aberration is the angle between the apparent solar wind direction and the

Earth–Sun line and is  $3^{\circ}$  on average. It is assumed that the instrument axis is pointing toward the aberrated solar wind direction to within a few degrees.

To meet these requirements, a variety of technologies must be considered, not only to build the instrument but also to operate it. In the present paper we address techniques for selectively sampling the energy and angular bins so as to cover only those voxels (velocity-space pixels) in energy-elevation-azimuth space where the solar wind beam is expected to be found. Indeed, at any given time only a fraction of all possible energy-elevation-azimuth voxels contain a significant number of particles. It

- 5 is therefore natural to sample the solar wind beam only around the expected energy and orientation, a process called "beam tracking". The purpose of this paper is to examine beam tracking strategies for electrostatic plasma analysers. Both energy tracking and angular tracking are considered (section 2). We describe how these strategies can be implemented (section 3). The performance of these strategies is then tested in section 4 with synthetic data, some of which are based on actual high-cadence solar wind data. A summary of the capabilities of beam tracking techniques and an outlook on other domains in which they
- 10 can be applied is presented in section 5.

#### 2 Beam tracking

Plasma spectrometers build up a VDF by detecting particles while scanning through three-dimensional velocity space. Plasma spectrometers typically gauge particles using an energy filter in the form of a quadrispheric electrostatic analyser (e.g. Carlson et al., 1982; Bame et al., 1992; Rème et al., 2001), although some new designs are emerging (e.g. Bedington et al., 2015; Ske

- 5 (e.g., Bedington et al., 2015; Skoug et al., 2016; Morel et al., 2017). Specifically relevant for beam tracking applications are spectrometers where an electrostatic elevation filter (using a transverse electric field set up between converging deflection plates) is placed in front of the analyser (e.g. McComas et al., 2007; Cara et al., 2017)(e.g., McComas et al., 2007; Cara et al., 2017)
   . Measurements are made over a range of azimuths simultaneously with a segmented anode array at the exit of the analyser. The particles are detected by means of a micro-channel plate or by channeltrons, each of which has its own advantages and
- 10 drawbacks.

The typical solar wind conditions at 1 au are well known from long-term statistical studies (e.g., Wilson III et al., 2018). Since the solar wind is usually supersonic and even super-Alfvénic (with rare exceptions, Chané et al., 2015), the solar wind thermal velocity (usually several 10s of  $\text{km} \cdot \text{s}^{-1}$  is well below the bulk velocity. In addition, the thermal energy is much less than the range of variation of the beam energies corresponding to slow and fast solar wind (see, e.g., Gosling et al., 1971; McComas

- et al., 2000, 2002). The solar wind speed vector can vary by 500 km·s<sup>-1</sup> and more near interplanetary shocks, and can reach up to 1500 km·s<sup>-1</sup> and more in interplanetary coronal mass ejections (e.g., Gosling et al., 1968; Volkmer and Neubauer, 1985; Dryer, 1994; Watari and Detman, 1998; Wu et al., 2016). Such dramatic changes occur over seconds to many minutes. The speed vector can change tangentially in solar wind discontinuities by > 100 km·s<sup>-1</sup> (see, e.g., Borovsky, 2012; Borovsky and Steinberg, 2014; Burlaga, 1969; De Keyser et al., 1998); the jump is
- 20 below  $\sim 65 \,\mathrm{km} \cdot \mathrm{s}^{-1}$  in 99% of the cases. Table 1 summarizes summarizes the implications of these numbers for the energies and solar wind arrival angles at 1 au (for a comparable exercise for heliocentric distances down to 0.23 au, see McComas et al., 2007). It is clear that the solar wind beam typically occupies only part of the energy-elevation-azimuth space that the instrument must be able to handle.

Beam tracking consists in making a prediction about the energy and orientation of the solar wind beam before one starts a

25 VDF measurement. Such a prediction may be obtained from the preceding measurements of the instrument itself, or may be based on data provided by other instruments (e.g., Faraday cup detectors) that can produce ion moment data at an even higher cadence; here the two variants are called "internal" and "external" beam tracking, respectively. Based on that prediction, the energy and angular windows can be defined over which the spectrometer has to scan to obtain the next VDF with minimum effort.

#### 30 2.1 Energy tracking

The energy range is essentially determined by the solar wind speed range and must go from  $< 600 \,\mathrm{eV}$  to  $\sim 20 \,\mathrm{keV}$ . The width of the energy window must cover at least 4 times the thermal proton energy. Since the energy range is usually discretised logarithmically (see below), the beam width should be at least 15% of the full log-energy range. However, a more stringent

requirement is that the energy window must be wide enough to avoid losing the solar wind beam upon sudden changes; depending on the VDF acquisition cadence, a width of 20–30 % of the full log-energy range seems to be a reasonable choice as will be shown below.

- The transmission properties of such an electrostatic analyser are such that only particles within a specified energy range  $\delta E$  are able to reach the detector, with a constant  $\Delta E/E$  defining the energy resolution of the instrument. It is therefore natural to divide the energy range logarithmically into  $N_E$  bins. A typical solar wind measurement does not necessarily have to scan all those bins, but may be limited to a number  $N_E^* \leq N_E$  corresponding to the energy window width derived above. "Energy tracking" then refers to intelligently choosing the bins that have to be scanned so that no significant parts of the energy distribution are left unsampled.
- 10 The total number of energy bins is fixed by the energy range to be covered, and by the energy resolution one wants to achieve, by

$$N_E = \frac{\log E_{\max} - \log E_{\min}}{\delta E/E}.$$

When performing energy tracking over an energy window of  $\Delta E$ , the number of energy bins to be sampled is only

$$N_E^* = \frac{\log(E + \Delta E/2) - \log(E - \Delta E/2)}{\delta E/E} \approx \frac{\Delta E}{\delta E}.$$

- 15 In general, one can choose both the centre of the energy window that has to be scanned and the width of that window. Changing the width of the window could be a way to take into account the changing temperature of the solar wind. It is, however, not recommended to do this. First, such decisions have to be made on-board and very fast, and deciding on the window width might be quite difficult if the VDFs have complicated shapes. Second, as discussed above, the width of the window is mostly determined by the need to handle rapid time variations. A third drawback is that this would make the duration of
- 20 VDF acquisition variable and thus unpredictable, which usually is considered undesirable from the point of view of on-board instrument management. This also is impractical for data handling.

Usually the VDF sampling is centred on the mean energy. Alternatively, it is possible to systematically shift the energy window upwards from the mean proton energy to minimise the chances of missing the peak of the He<sup>++</sup> contribution, which for the same mean velocity has an energy-over-charge that is twice that of the dominant proton population; in such an  $\alpha$ -particle operating mode, the number of energies in a scan has to be large enough to include the proton and  $\alpha$  peaks with

sufficient margin (for THOR-CSW design,  $N_E^* \ge 24$ , so that the energy range spans at least a factor of 5.6).

#### 2.2 Angular tracking

A similar reasoning applies to the angular range of the solar wind beam. The thermal beam width suggests a minimum sampling width of  $24^{\circ}$ , centred around a solar wind arrival direction that can vary within a certain range around the average aberrated

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solar wind direction (Fairfield, 1971), as indicated in Table 1. In general,  $N_{\theta}^* \leq N_{\theta}$  and  $N_{\alpha}^* \leq N_{\alpha}$  for elevation and azimuth, respectively.

The use of wider windows may help to avoid missing temperature anisotropy effects in the VDFs (Marsch et al., 2006; Marsch, 2012) or the presence of suprathermal beams and/or extended plateaus in the VDFs (Marsch et al., 2009; Osmane et al.,

2010; Marsch, 2012; Voitenko and Pierrard, 2013). Beam tracking strategies follow essentially the core of the distribution. In order not to miss features that may appear outside of the thermal wind advection cone, the actual energy–elevation–azimuth windows selected for data acquisition must be large enough.

#### 2.3 Theoretical speed-up

5 Scanning the complete set of energies, elevations, and azimuths requires a time

$$\Delta t_{\rm full} = N_E N_\theta N_\alpha \delta t / N_{\rm par}$$

where  $\delta t$  is the time needed for accumulating particle detections in a single energy–elevation–azimuth bin, and  $N_{\text{par}}$  is the number of bins that are sampled simultaneously. In the THOR-CSW design, for instance, all azimuths are sampled in parallel by having a dedicated anode for each azimuth, so that  $N_{\text{par}} = N_{\alpha}$  (Cara et al., 2017). Scanning only the set of energies, elevations, and azimuths identified by the beam tracking strategy, requires

$$\Delta t = N_E^* N_\theta^* N_\alpha^* \delta t / N_{\text{par}}.$$

10

The theoretical speed-up achieved by beam tracking then is

$$G = \frac{\Delta t_{\text{full}}}{\Delta t} = \frac{N_E}{N_E^*} \frac{N_\theta}{N_\theta^*} \frac{N_\alpha}{N_\alpha^*}$$

corresponding to the fraction of VDF voxels that is sampled during each measurement cycle. Taking the THOR-CSW design 15 as an example, a full energy-elevation-azimuth scan would have  $N_E = 96$ ,  $N_\theta = 32$ ,  $N_\alpha = 32$ . The standard energy tracking mode has  $N_E^* = 16$ ,  $N_\theta^* = N_\theta$ ,  $N_\alpha^* = N_\alpha$ , so that G = 6. The standard combined energy and elevation tracking mode has  $N_E^* = 16$ ,  $N_\theta^* = 16$ ,  $N_\alpha^* = N_\alpha$ , so that G = 12, i.e., an order of magnitude improvement in time resolution can be achieved. In reality, the speed-up may be somewhat less since for angular beam tracking the importance of the settling times needed when changing the high voltages on the analyser plates is relatively higher (there are more frequent deflector voltage scans, while they

- 20 are shorter). Note that the voltages on the deflector plates can be swept in a continuous manner, avoiding settling times except at the start of an elevation scan, which coincides with the start of an energy step (Cara et al., 2017). For example, a VDF obtained from sampling all  $N_E \times N_\theta \times N_\alpha = 98304$  voxels with an integration time of  $\Delta t_{int} = 0.180$  ms and a high voltage settling time of  $\Delta t_{hv} = 0.200$  ms would take  $\Delta t_{full} = N_E (N_\theta \Delta t_{int} + \Delta t_{hv}) = 573$  ms, given that all azimuths are acquired simultaneously. Energy tracking alone would sample  $N_E^* \times N_\theta \times N_\alpha = 16384$  voxels in  $\Delta t = N_E^* (N_\theta \Delta t_{int} + \Delta t_{hv}) = 95.4$  ms, exactly G = 6
- times faster than a full scan. Combining energy and elevation tracking leads to sampling  $N_E^* \times N_{\theta}^* \times N_{\alpha}^* = 8192$  voxels in only  $\Delta t = N_E^* (N_{\theta}^* \Delta t_{int} + \Delta t_{hv}) = 50$  ms. The resulting speed-up is  $\Delta t_{full} / \Delta t = 11.5$ , slightly less than the expected G = 12.

#### **3** Beam tracking strategies

The potential speed-up provided by beam tracking comes at a cost: There is a risk that one misses (part of) the solar wind beam. The reason is that one has to predict, at the start of a measurement cycle, where the beam is to be found. Such a prediction

30 necessarily is prone to error. Therefore, one has to devise a beam tracking strategy that is robust.

#### 3.1 Computing mean energy and arrival direction

As discussed above, beam tracking boils down to predicting the average velocity or energy of the solar wind beam, and its arrival direction. The energy, elevation, and azimuth sampling windows are then shifted so that they stay centred around the predicted value.

5 Let us consider internal beam tracking first. During VDF measurement cycle p, the instrument scans through a contiguous subset of the energies  $E_i$ ,  $i = i_p, ..., i_p + N_{Ep}^* - 1$ , of the elevations  $\theta_j$ ,  $j = j_p, ..., j_p + N_{\epsilon p}^* - 1$ , and azimuths  $\alpha_k$ ,  $k = k_p, ..., k_p + N_{\alpha p}^* - 1$ , to obtain a distribution function  $f(E_i, \theta_j, \alpha_k)$ . Based on these measurements, one can determine the energy distribution by summing over the elevation and azimuth bins

$$f_E(E_i) = \sum_{j=j_p}^{j_p + N_{\theta p}^* - 1} \sum_{k=k_p}^{k_p + N_{\alpha p}^* - 1} \gamma_{ijk} f(E_i, \theta_j, \alpha_k),$$

- 10 where the γ<sub>ijk</sub> are known factors that incorporate instrument geometry, detector gain, and detector ageing coefficients. Note that the energy distribution can be constructed progressively as the scans over energy, elevation, and azimuth are performed. The mean or peak energy (E)<sub>p</sub> can be readily derived from this energy spectrum; the former is considered to be a bit more robust than the latter. One can proceed in a completely analogous way to obtain the mean or peak elevation and azimuth.
- The above description is actually a simplification that is applicable only to 3-axis stabilised or slowly rotating spacecraft.
  15 If the spacecraft spin phase changes significantly during the measurement, the construction of the VDF becomes more complicated as the attitude changes have to be accounted for; this is a task that usually is performed on-ground. Beam tracking, however, requires the mean energy and arrival directions to be established on-board and fast. First, one can simply assume that the spacecraft spin rate is sufficiently low. For the THOR-CSW case, the spin phase change should be less than Δω = arctan(1.5°/24°) = 3.6° during the acquisition of a VDF in order not to lose the desired angular resolution. Knowing
- that THOR was planned to spin at 2 rpm, the VDF acquisition time should be less than  $\sim 300 \text{ ms}$ . In practice, this condition may be somewhat too strict since most data are gathered near the centre of the sampled range. In any case, the faster a VDF is assembled, the less such rotational smearing effects; the use of beam tracking helps to ensure that this condition is satisfied. There is a simple way, however, to relax the above limitation. Rather than computing the energy distribution over the whole set of energies that have to be scanned, the set can be divided in a number of chunks, each of which covers only
- 25  $N_{\text{chunk}} \ll N_E^* \leq N_E$  energy channels. In the case of THOR-CSW, the choice  $N_{\text{chunk}} = 8$  was considered. A full energy scan would therefore require  $N_E/N_{\text{chunk}} = 12$  chunks, while a 16-energy scan requires 2 chunks. The (partial) moments are computed for each chunk and then combined to obtain the full moments while taking into account the spacecraft spin. Such an operation is much simpler than a full correction for spin at the level of the individual energy–elevation–azimuth voxels. It is convenient because the computations for each chunk can be done in parallel with the data acquisition for the next chunk. But
- 30 most importantly, the condition for avoiding rotational smearing applies to the acquisition of a chunk, rather than of the full VDF. The time needed to collect a chunk with 8 energies and 16 elevations is 25 ms, and that for a chunk with 8 energies and 32 elevations is 48 ms, which both are well below the  $\sim 300 \text{ ms}$  limit found above. This offers a viable and straightforward way to compute the mean energy and arrival directions needed for internal beam tracking on-board. The same type of computation

can provide all on-board plasma moments, which is particularly useful if only a fraction of all full VDFs can be transmitted to the ground due to telemetry limitations; this enables the implementation of a survey data mode that provides only the on-board moments with good quality.

External beam tracking is an interesting option when another instrument is available that provides plasma moments at a 5 higher speed than the plasma spectrometer, such as a Faraday cup instrument (e.g. Šafránková et al., 2013)(e.g., Šafránková et al., 2013)

- . Such instruments can provide solar wind speed and velocity direction (and thermal velocity), from which the settings for the next measurement cycle can be derived. Usually, the arrival direction is known in that instrument's reference frame. One then needs to know its alignment relative to that of the plasma spectrometer to be able to translate these measurements into usable values for the beam tracking procedure onboard. Finally, also the delay time between data acquisition and use in the plasma
- 10 spectrometer must be known. The acquired data receive a time stamp from the clock of the auxiliary instrument, which must be synchronised to the same reference as the plasma spectrometer's clock. The delay time includes computation time in the auxiliary instrument and the time needed for transmission, possibly via the payload processor; it obviously should be minimal.

#### 3.2 Prediction

The decision on which part of phase space to scan in the upcoming measurement cycle is always a matter of prediction. The simplest form of prediction is just taking the value from the last measurement. For instance, if the previous cycle p resulted in an average energy  $\langle E \rangle_p$ , one can choose the <u>center centre</u> of the energy range for cycle p + 1 as

$$E^{(p+1)} = \langle E \rangle_p,$$

i.e., one uses zero order (constant) extrapolation. A slightly more advanced prediction is obtained through first order (linear) extrapolation:

20 
$$E^{(p+1)} = 2\langle E \rangle_p - \langle E \rangle_{p-1}.$$

Second order (parabolic) extrapolation results in

$$E^{(p+1)} = 3\langle E \rangle_p - 3\langle E \rangle_{p-1} + \langle E \rangle_{p-2}.$$

In principle one may even use higher-order polynomial extrapolation. There are, however, a number of drawbacks. In general, n-th order extrapolation requires n + 1 preceding values. The underlying assumption of polynomial extrapolation is that the

25 behaviour of  $\langle E \rangle(t)$  is smooth (*n* times continuously differentiable) during this whole  $(n+1)\Delta t$  time period; if not, the extrapolated value may be completely off the mark. Such smoothness is questionable in the solar wind at shocks or discontinuities, so a high *n* is not warranted. All in all, one can expect such higher-order interpolation techniques to work reasonably well only if the energy does not change rapidly, but in such cases a low order extrapolation works fine too.

Also, if any of these values happens to be corrupted (e.g., by a single event upset in one of the anodes or in the ADC electronics), the prediction can be wrong. In order to eliminate values that are completely offoutliers, a voting mechanism can be used. Consider the three last measurements, and compute  $|\langle E \rangle_p - \langle E \rangle_{p-1}|$ ,  $|\langle E \rangle_p - \langle E \rangle_{p-2}|$ , and  $|\langle E \rangle_{p-1} - \langle E \rangle_{p-2}|$ .

Identify the smallest of these three differences. It can be assumed then that this smallest difference corresponds to two values that are not corrupted as they seem to agree with each other. One can then perform constant extrapolation by adopting the most recent of those two numbers as  $E^{(p+1)}$ . Alternatively, one can perform linear extrapolation with those two values. Note that such a more robust procedure requires one more a voting mechanism requires an additional preceding value, implying that

5 the prediction may rely on information that is somewhat older. In other words, the ability of the algorithm to cope with rapid changes in the solar wind VDFs is slightly degraded.

One way of implementing (internal or external) beam tracking is by storing the  $\langle E \rangle_p$  measurements, together with their time tag, in a first-in first-out queue. As soon as the instrument is ready for setting up the next VDF acquisition, the most recent measurements are retrieved to make a prediction. This asynchronous system always works, even when there are processing

10 delays associated with the interpretation of previously obtained VDFs (for internal beam tracking) or with the processing and transmission of the data of the driving instrument (for external beam tracking). Such asynchronicity is also useful if the VDF acquisition cycle has a variable duration, e.g., when the number of sampled energy bins is variable.

The procedure outlined above also holds for angular tracking. There is one additional complication, though, in that all azimuth-elevation pairs must be rotated along with the spacecraft spin. Not doing so would lead to systematic offsets in predicted beam position, which can be neglected only for slowly rotating spacecraft.

An argument in favour of external beam tracking is that such an instrument may offer more recent data to base a prediction on. Nevertheless, it is important to note that, conceptually, internal beam tracking can always be considered "good enough". Indeed, a prediction based on the previous plasma spectrometer measurement involves an extrapolation over a time interval roughly equal to the VDF acquisition time. This would not be justified if the solar wind would change significantly over such an interval. But if that is the case, the time resolution of the spectrometer is simply insufficient and the VDFs that are acquired are questionable anyhow since they involve sampling a changing distribution. A posteriori verification is always possible by

comparing subsequent VDFs.

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#### 3.3 Beam loss detection and recovery

The desire for a robust prediction stems from the fact that the internal beam tracking process suffers from a self-destructive property: if a prediction is off the mark, the next measurement cycle will not correctly represent the VDF, so that the subsequent prediction is extremely likely to be worthless. In other words, once one starts having difficulties with tracking the beam, one will rapidly miss it completely and possibly indefinitely.

One therefore needs a system for recovery of the beam. A straightforward and failsafe mode of operation is by regularly performing a scan over the entire energy–elevation–azimuth range. In this way, if one loses the beam, one is sure to pick it up again after a finite time interval. More sophisticated strategies could examine the shape of the obtained VDF to check whether part of the VDF is missed. Implementing such sophisticated strategies on-board, however, is difficult and it is hard to ensure that they are robust (i.e., when there is beam loss, the strategy should indicate this) and efficient (i.e., when the strategy indicates that there is beam loss, that should actually be the case so that a beam recovery action is needed). In the present study we have adopted a simple condition: if the measured density is below a threshold  $n_{\text{beam-loss}} = 0.1 \text{ cm}^{-3}$ , the beam is considered to



**Figure 1.** Plasma spectrometer measurements of a constant Maxwellian solar wind beam on a rapidly spinning spacecraft using internal energy and elevation beam tracking. From top to bottom: the energy spectrum of the Maxwellian solar wind; the energy spectrum as acquired by the plasma spectrometer at t = 3.95 s with the vertical black and green dashed lines indicating the centre and the bounds of the sampled energy range; the energy as a function of time, where the horizontal blue line represents the true solar wind value, the small red dots are the Faraday cup measurements every 30 ms (not used with internal beam tracking), the magenta circles and triangles indicate the centre and the bounds of the sampled energy range, and the red diamonds give the mean energy as determined by the plasma spectrometer; the azimuth (same format, no beam tracking for azimuth); the elevation (same format); and the spin phase. The panels at the right hand side show the energy–elevation, energy–azimuth, and azimuth–elevation projections of the VDF at t = 3.95 s. See the main text for more details.

be lost. The recovery action is to scan over the entire instrument range once or several times, depending on the extrapolation method, to restart the beam tracking process. In fact, this is exactly how the beam tracking strategy is initialised in the first place.

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A situation that could be particularly troublesome is that of very low solar wind densities and/or high temperatures, e.g., downstream of a strong shock propagating through an already tenuous solar wind. In such situations the count rates are low, so that the signal-to-noise ratio might be reduced. This could inadvertently trigger a "beam loss" condition. The consequences of that would, however, not be dramatic: the instrument simply returns to a measurement strategy that samples the full instrument range, and it would keep doing so for as long as the low density condition holds. Although one would lose time resolution, providing VDFs over the full instrument range is one of the best things one can do in such a situation (especially for the high

temperature case). A posteriori, one can still bin the measurements in energy, azimuth, elevation and/or time to improve the signal-to-noise ratio even further so that these measurements can become scientifically useful. It should also be noted that beam tracking driven by a Faraday cup instrument would suffer less from problems in such situations, since a Faraday cup inherently provides a better signal-to-noise as it integrates the particle flux over its entire field of view.

- 5 Beam loss is especially problematic if one is not able to downlink the full VDFs, but only moments that are computed on-board. In that case one has no means whatsoever to assess the reliability of the moments, since parts of the VDF might have been missed. It is then advised to downlink a subset of the VDFs, though at a much slower rate, to at least allow a regular check on the proper functioning of the beam tracking strategy. Alternatively, one may downlink reduced distributions, e.g., the energy and angular distributions  $f_E(E_i)$ ,  $f_{\theta}(\theta_i)$  and  $f_{\alpha}(\alpha_k)$ , to ascertain that no significant part of the population has been missed.
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#### Physical underpinning 3.4

Losing the beam is definitely to be avoided if one aims for continuous and reliable solar wind measurements. The key question is: how rapid is the instrument VDF sampling compared to the variability in the solar wind?

- An A partial order-of-magnitude answer to this question is can be obtained by considering the following qualitative argument. Spatial variations in the jon distributions eannot be much smaller than are often characterised by the jon gyroradius. 15 which is on the order of  $100 \,\mathrm{km}$  in the solar wind at 1 au. A steady plasma discontinuity of such thickness that passes by the observer with a (fast) solar wind speed of  $1000 \,\mathrm{km \cdot s^{-1}}$  and with the discontinuity normal aligned with the flow direction (the most pessimistic situation), is seen by the observer as a time variation over 100 ms. In order to track abrupt changes at that time scale, a measurement time resolution of  $\sim 10 \,\mathrm{ms}$  should be sufficient. Note that in shocks, for instance, the ion distributions can
- vary on the electron scale (Mazelle et al., 2010; Krasnoselskikh et al., 2013), which would require a time resolution that is at 20 least an order of magnitude better.

Another way to address this question is to look at some of the highest-cadence solar wind measurements ever made. Data from the Bright Monitor of Solar Wind (BMSW) experiment on the Spektr-R mission (Šafránková et al., 2013) indicate shock ramps that last only 200 ms. A statistical analysis by Riazantseva et al. (2015) shows that the solar wind fluctuation spectrum becomes quite flat around 10 Hz, indicating that rapid intermittent variations with rather large amplitude are fairly common.

One arrives at the conclusion that rapid variations do occur and that beam tracking works best for sampling frequencies of 10-100 Hz or smaller. If the plasma spectrometer succeeds in sampling the VDFs at such a high cadence, there is little risk for beam loss.

#### Performance 4

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In this section different strategies for beam tracking are evaluated by means of a software simulator of the THOR-CSW 30 instrument.



Figure 2. Plasma spectrometer measurements of a constant Maxwellian solar wind beam on a spinning spacecraft using internal energy and elevation beam tracking. The plot shows the maximum deviations  $\Delta \alpha$  and  $\Delta \theta$  between the spectrometer's mean azimuth and elevation and the solar wind azimuth and elevation of the spacecraft spin period  $t_{spin}$ .

#### 4.1 Beam tracking on a spinning spacecraft

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As a first test, consider a constant solar wind proton beam in the form of an isotropic Maxwellian distribution, with a speed that does not coincide with the solar direction (i.e., with the spin axis of the spacecraft). We ignore here the issue of aberration. As the spacecraft spins, the beam appears to trace a circle around the spin axis in the spectrometer field of view. Angular beam tracking can then be used to follow this ever-changing apparent arrival direction. We consider a solar wind beam with a density of 5 particles  $cm^{-3}$ , a velocity of  $[-400, 100, 0] \text{ km} \cdot \text{s}^{-1}$  in GSE coordinates, an isotropic temperature of  $10^5$  K, and a spacecraft spin period of 2 s. Internal energy and angular beam tracking are used with constant extrapolation.

Figure 1 shows the results of the simulation (see Supplementary Materials for animations of all the simulations presented in this paper). The instrument is initialised at time t = 0 ms. It starts measuring a first VDF over all energies and all angles

10 at t = 600 ms, an operation that lasts almost 600 ms. The mean energy, azimuth and elevation are determined; note that these measurements are associated with the middle of the time interval during which the VDF is acquired. The mean energy and elevation then are used to start energy and elevation beam tracking. For the energy, the beam tracking procedure is useful at the beginning to find the appropriate energy range; as the beam energy remains constant, the energy sampling interval does not change any more. The elevation, however, changes sinusoidally. As can be seen in the figure, the beam is tracked very



Figure 3. Plasma spectrometer measurements of a constant solar wind beam from a spacecraft with spin period  $t_{spin} = 0.25$  s. The plot layout is the same as that of Fig. 1.

well, thanks to the prediction that takes the spacecraft rotation into account. Note that the centre of the sampled elevation range cannot follow the measured mean elevation when the upper or lower bound of the range coincide with the spectrometer's upper or lower elevation limit, but as long as the difference is small and the beam fits into the scanned range, there is no problem. The difference between the solar wind arrival angles and the As an indication of the quality of the beam tracking scheme, we find that the measured mean azimuth and elevation remains below do not differ more than 0.6° from the the solar wind arrival

angles with which the simulation is set up, well within the 1.5° discretisation error.

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There is no risk for losing the beam in energy or elevation as its position in energy–elevation–azimuth space is constant when compensating for the spacecraft spin. It is interesting to see what happens if the spin rate changes. Variants of the above example have been simulated for  $t_{\rm spin}$  from 0.25 to 2 s; for each of these, the maximum azimuth and elevation deviations have

10 been evaluated over a full spin (while ignoring possible transient effects during the initialisation of the beam tracking mode). As Fig. 2 shows, the deviations become larger as the spacecraft spins faster. For example, with a spin period of only 0.25 s (see Fig. 3), the 50 ms time needed to collect a VDF is too large to justify the hypothesis that the solar wind does not change in the meantime (in the spacecraft frame of reference). Consequently, the collected distributions are somewhat distorted. Such



**Figure 4.** Plasma spectrometer measurements during the passage of a gradual plasma discontinuity (duration 500 ms) using internal energy and elevation beam tracking. The plot layout is the same as that of Fig. 1.

"rotational smearing" affects the measured solar wind arrival direction, but not the energy spectrum. The distortion represents an apparent increase in the temperature anisotropy. Nevertheless, the beam tracking process still works fine.

#### 4.2 Beam tracking at a plasma discontinuity

- In a second test the response of the plasma spectrometer to the passage of a plasma discontinuity is examined. The discontinuity is characterised by a transition in proton properties as the density changes from 5 to 1 particles  $\cdot$  cm<sup>-3</sup> and the isotropic temperature from 10<sup>5</sup> to 4×10<sup>5</sup> K, while the velocity jumps from [-400, -50,0] to [-800,0,100] km  $\cdot$  s<sup>-1</sup> in GSE coordinates. The transition is centred at t = 2 s and has a duration  $\Delta t_{\text{disc}} = 500$  ms. The spacecraft spin period is 30 s but does not really matter here. Internal energy and angular beam tracking are used with constant extrapolation. The simulation in Fig. 4 demonstrates how both energy and angular beam tracking work in unison to flawlessly follow the solar wind beam as it changes its direction
- 10 and as its energy increases by a factor of 4 through the transition. If one would have sampled over the full energy–elevation– azimuth ranges, there would have been only 1 or 2 measurements during the passage of the discontinuity, while there are  $\sim 10$ measurements when using beam tracking.



**Figure 5.** Plasma spectrometer measurements during the passage of an abrupt plasma discontinuity (duration 50 ms) using internal energy and elevation beam tracking. The plot layout is the same as that of Fig. 1.

The simulation in Fig. 5 repeats the previous example, but now for  $\Delta t_{\text{disc}} = 50 \text{ ms}$ . Given that the beam changes its energy considerably and abruptly, a situation of beam loss occurs during the transition. This is due to the energy change, not due to the elevation change. The instrument has begun scanning over the lower energy channels at the time the solar wind velocity is ramping up rapidly, so that the solar wind beam has disappeared from the higher energy channels in the scan. This leads to an underestimation of the density, and to a decrease of the mean energy so that the next VDF measurement cycle is completely off. Missing the beam leads to a measured density that is less than the 0.1 particles  $\cdot \text{ cm}^{-3}$  threshold, triggering the beam loss condition at the end of acquiring the data point at 00:00:02.050 (collection between 00:00:02.025 and 00:00:02.075). The figure shows the beam recovery strategy jumping into action by first doing a full scan to find the beam again at 00:00:02.365 (data collected between 00:00:02.075).

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In order to explore the limits of beam tracking as the discontinuity time scale becomes shorter, the maximum density and energy errors (deviation of the measured moments from the solar wind value) are evaluated as a function of  $\Delta t_{\text{disc}}$  and are presented in Fig. 6. The top panel in the figure indicates whether or not beam loss occurs (true or false, respectively). When there is beam loss, the density is erroneous by definition since it is below the threshold there. Note that the error may already be



Figure 6. Plasma spectrometer measurements during the passage of a plasma discontinuity. The spectrometer uses internal energy and elevation beam tracking. The plot shows the occurrence of beam loss (true or false) and the maximum deviations in plasma density, energy, azimuth, and elevation between the measured values and the true solar wind values that occur throughout the passage, as a function of the discontinuity crossing duration  $t_{disc}$ . The measurements are more accurate as the plasma property changes associated with the discontinuity occur over a longer time scale.

important even when the beam loss condition is not triggered yet. The energy, azimuth and elevation errors also systematically increase for a more rapid transition. While the maximum azimuth and elevation errors remain  $\leq 0.75^{\circ}$  (half of the 1.5° the angular resolution) as long as there is no beam loss, the maximum energy deviation is around 100%, which is not surprising since the beam is lost because it moves out of the energy range. The measurement points measurements right before beam

5 loss can thus be erroneous as part of the distribution may already be missed. One might fit an analytical distribution function (Maxwellian, bi-Maxwellian, Lorentzian) to the observed VDF to try to compensate for that. In any case, a look at the VDF will help in identifying that there has been an issue and to ascertain that a part of the VDF has not been measured.

In conclusion: Beam tracking can deal with progressive changes over a time scale longer than the sampling time, regardless the magnitude of the change. For shorter time-scale changes, there is no problem as long as the changes are not very large so that the beam still fits in the energy and angular windows.

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**Figure 7.** Plasma spectrometer measurements for a solar wind simulation based on BMSW on Spektr-R observations on 2014-06-08, using internal energy and elevation beam tracking. The plot layout is the same as that of Fig. 1, but also shows density,  $\frac{GSE}{GSE}$ -velocity in the spacecraft frame of reference (including spacecraft spin, x axis pointing to the spacecraft's orbital motion around EarthSun, and spacecraft spinning in the Earth's motion around the Sunx-y plane), and temperature, as a function of time.

#### 4.3 Beam tracking for fast solar wind measurements

In the previous examples, synthetic data have been used to understand the possibilities and limitations of beam tracking. We now try to perform more realistic tests. Since no full solar wind VDF measurements have ever been made at such a rapid

cadence, we have to create hypothetical solar wind data. This is done by using the aforementioned high-cadence solar wind measurements from the BMSW experiment on the Spektr-R mission (Šafránková et al., 2008, 2013). The moments from that instrument, expressed in GSE coordinates and with a time resolution of  $\sim 31 \text{ ms}$ , have been used to construct Maxwellian proton distributions, and the resulting VDF time sequence has been used as the "true solar wind" sampled by the plasma spectrometer.

- 5 A simulation is shown in Fig. 7 for BMSW measurements on 2014-06-08 exhibiting moderate changes in solar wind direction; there is little variation in density, energy, and some variability in temperature. The instrument is perfectly capable of following these changes since these are neither dramatic in magnitude nor-or very abrupt as they occur over time scales of seconds. Indeed, there do not seem to be discontinuous variations in the BMSW data, implying that solar wind variability takes place mostly over time scales of a multiple of  $\sim 31 \text{ ms}$ .
- A more challenging situation is presented in Fig. 8. The BMSW instrument observes a strong shock around 2015-06-22 18:28:22 UT, where the velocity changes from 400 to  $700 \,\mathrm{km \cdot s^{-1}}$ , accompanied by solar wind direction changes, and by density and temperature enhancements by a factor of 2 to 3. The variations are both large and fast. The Faraday cup measurements at this time were performed using sub-optimal high-voltage settings that lead to an overestimation of velocity and temperature and an underestimation of density; the velocity overshoot up to  $900 \,\mathrm{km \cdot s^{-1}}$  is likely unphysical. In the present exercise we ignore
- 15 these data reliability issues and blindly feed the simulation with the Faraday cup moments. It turns out that the beam tracking procedure works perfectly. While the solar wind energy changes significantly in about 2 seconds, this change occurs stepwise and with the instrument's 50 ms time resolution there are sufficient intermediate samples to follow the energy enhancement. The beam direction shows rapid changes between 18:28:18 and 18:28:22 UT and between 18:28:33 and 18:28:38 UT, and these too are well tracked.
- 20 Although beam tracking works well, several problems are apparent. First, the  $[-24^\circ, +24^\circ]$  elevation and azimuth ranges are sometimes too small. For instance, the solar wind beam elevation reaches  $+20^\circ$  around 18:28:13 UT, which is too close to the limits of the instrument, and the solar wind azimuth effectively goes beyond the  $-24^\circ$  limit around 18:28:21 UT. In both cases, part of the solar wind beam is missed. Especially for the latter this leads to an error on the measurement, especially for the density. Such strong angular deviations are rare, but that makes these situations particularly interesting from the scientific
- 25 point of view. Note also that situations in which the beam leaves the instrument field of view will occur even more often if there is a deviation of the pointing of the instrument (i.e. of the spacecraft it is mounted on) from the solar direction. A second issue is that the solar wind distribution changes too abruptly during the most rapid parts of the transitions around 18:28:22 the solar wind distribution changes too abruptly so that the VDF is mixed up (especially apparent in the animated version of the simulation in the Supplementary Materials), leading to incorrect density and temperature measurements. This situation is
- 30 at the limits of the transition time scale inferred in section 3.4: the magnetic field can be strong near interplanetary shocks , and so the gyroradius might be relatively small; combined with a large speed ,, there can be electron-scale structure, and in combination with the large speed this can lead to short time scales. A third second problem is that around 18:28:22.5 the solar wind temperature is at moments so high that the beam becomes too broad to be captured completely in the sampling window; the density and the temperature as determined by the instrument are therefore somewhat too small. Sampling the solar wind
- 35 without beam tracking every 600 ms partially avoids the high temperature issue, but the assumption that the VDF does not

change during the sampling interval would be justified even less. All solar wind measurements up to now have had to contend with that. The speed-up from beam tracking appears to be essential to overcome this difficulty.

In the above examples, the emphasis was on the question whether the beam tracking technique is able to follow the rapid solar wind variations, which essentially were rapid variations of the plasma moments. However, there may equally well be

5 rapid changes in the shape of the VDFs (which we do not know since BMSW only provides the moments). The examples presented here therefore can only be considered as partial tests.

#### 4.4 Internal and external beam tracking

The 50 ms time resolution of the plasma instrument with energy and elevation tracking described above is of the same order as that of a typical Faraday cup instrument. In that situation, there is little to be gained by using external rather than internal beam
tracking. If one decides to run the plasma instrument using energy tracking only (16 energies, 32 elevations), for instance, in order to keep a field of view that is as wide as possible, the time resolution is ~100 ms, i.e., significantly slower, and then external beam tracking becomes attractive. This situation is shown in Fig. 9 for an assumed delay time (time between centre of Faraday cup measurement and the moment that it is available for the plasma spectrometer) \Deltateq t<sub>delay</sub> = 30 ms. The error on the Faraday cup measurements should be on the order of the spectrometer energy and angular resolution at most. The hypothesis

- 15 made here is that they are exact. Again, beam tracking works well, but the risk of time variability below the VDF acquisition time scale is even larger than before. This illustrates the fundamental limitation of external beam tracking. Fast VDF acquisition is needed both to avoid variability while acquiring a VDF, and to have a reliable prediction for beam tracking thanks to a short prediction horizon. External beam tracking only addresses the second issue. An advantage of external beam tracking is that beam loss cannot occur and a recovery strategy is not needed: If the instrument keeps following the guidance from the Faraday
- 20 cups (and assuming that these produce accurate results), it will always recover the beam, even if the beam has disappeared from the instrument field of view for some time.

#### 5 Conclusions

Beam tracking is an important element in the observational strategy of plasma spectrometers that try to provide high-cadence solar wind ion VDFs for in-depth studies of the behaviour of the plasma and its response to turbulence at kinetic scales. It
is an essential tool to guarantee optimal energy and angular resolution, without compromising the signal-to-noise ratio, with minimal VDF acquisition time. It requires the VDF acquisition rate to be fast enough so that the beam energy and direction do not change dramatically within the acquisition time interval. At the same time, trustworthy run-time predictions of beam energy and direction must be available, either from the previous measurements (internal beam tracking) or from another instrument (external beam tracking). We have explored the performance of various beam tracking strategies using synthetic and actual

30 data from the Spektr-R/BMSW instrument. It turns out that the approach works well, but may fail at times, so that a robust beam recovery mechanism must be planned (for the case of internal beam tracking).



**Figure 8.** Plasma spectrometer measurements for a solar wind simulation based on BMSW on Spektr-R observations of a strong shock on 2015-06-22, using internal energy and elevation beam tracking. The plot layout is the same as that of Fig. 7.

It appears that solar wind variations can at times be extremely rapid, as for the interplanetary shock observed on 2015-06-22 around 18:20:22 UT by the Spektr-R/BMSW instrument, therefore requiring a high time resolution. The simulation experiments conducted here show that a time resolution of 50 ms is sufficient for most situations, but at some fast shocks this is apparently not fast enough. In view of considerations regarding the proton gyroradius, is seems likely that a resolution of  $\sim 10$  ms would be sufficient, but at present data at a 100 Hz cadence are not available to verify this.

5



**Figure 9.** Plasma spectrometer measurements for a solar wind simulation with the same data as Fig. 8, using external energy beam tracking with a delay of 30 ms. The plot layout is the same.

It is always advised to perform regular diagnostics to check whether the beam tracking strategy is working properly. This can be done by examining the VDFs that are recorded, from which it may be apparent that part of the solar wind beam is missing. It is therefore desirable to have a Faraday cup instrument and a plasma spectrometer working in tandem. Even though the usefulness of external beam tracking is limited, the Faraday cup measurements can be used for cross-calibration, to verify whether the beam does not move out of the field of view (partially or completely) and to assess whether beam loss

has occurred (especially in situations where only the plasma spectrometer moments are available), and to verify whether the plasma distribution did not dramatically change while the spectrometer was acquiring a VDF.

Beam tracking is not to be confounded with a posteriori peak tracing as used on the Helios-1 and -2 spacecraft (Rosenbauer et al., 1977, 1981). Peak tracing consists in searching for the main peak position in an acquired VDF, which typically contains

5 many voxels with little or no counts in case no beam tracking is used. One may then choose to retain only that part of the distribution function for downlink. Even if one does not perform such a peak search, modern data compression techniques are able to exploit the presence of empty bins to reduce the data volume efficiently. Beam tracking itself already provides such a data compression simply by not measuring irrelevant regions of energy–elevation–azimuth space.

An outcome of the simulations presented here is that a field of view of  $48^{\circ} \times 48^{\circ}$  (as originally foreseen for THOR-CSW

- 10 (Cara et al., 2017)) tends sometimes appears to be a bit narrow. Enlarging the field of view would lead to a degradation of angular resolution (for the same number of azimuth and elevation bins), but a 2° angular resolution and a 64°×64° field of view could be an interesting choice that simultaneously mitigates the problem of partially missing the beam when the solar wind velocity is is very hot and/or the flow is strongly non-radial, deals with hot solar wind situations, and reduces the risk of beam loss when the solar wind arrival direction changes rapidly. Such a wider field of view also relaxes the constraint that the
- 15 instrument should be pointing accurately to the average (aberrated) solar wind direction; allowing the pointing direction to be off by several degrees reduces the frequency of spacecraft attitude change manoeuvres. The downside is that deflection over large angles is difficult to achieve while respecting the desired angular resolution.

A fast solar wind beam tracking spectrometer is particularly useful if, on the same spacecraft, it is combined with an omnidirectional spectrometer. The synergy between both allows to acquire high cadence solar wind beam distributions together

20 with the omnidirectional context at a lower cadence. Comparison between the data from both instruments can help to detect situations where the picture provided by the beam tracking instrument is insufficient to completely characterise the plasma environment, including for instance reflected ions from interplanetary shocks. Note that a slower instrument can also feature a mass resolution capability, which could help to identify the alpha particle contribution in the beam tracking VDFs.

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It is possible to regard beam tracking as a form of "sparse sampling" or "compressed sensing" (see Donoho, 2006; Donoho et al., 2006, and . More advanced applications from this active area of research might allow further improvements in VDF acquisition speed.

That a sparse representation of VDFs can be useful is demonstrated in Vlasov simulations (e.g., through enhancing sparsity by ignoring pha . Their practical applicability to accelerate plasma spectrometer measurements remains to be proven.

While beam tracking is extremely well suited for solar wind monitoring, it can be used in other contexts as well. A possible application would be to apply energy and angular beam tracking for focusing on the details of precipitating and upwelling

30 ion or electron beams in the auroral regions: such beams typically are narrow in angular extent as they tend to follow the magnetic field, and they are nearly mono-energetic with an energy that can range from a tens of eV up to  $\sim 10 \text{ keV}$ , at least for electrostatically accelerated particles.

*Data availability*. Movies (in MP4 format) that illustrate the beam tracking simulations described in this paper are provided as supplementary material under doi:10.18758/71021039 at *http://repository.aeronomie.be/?doi=10.18758/71021039*. The Spektr-R/BMSW high resolution solar wind data can be obtained from *https://aurora.troja.mff.cuni.cz/spektr-r/*.

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